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FINAL PROJECT REPORT

Estimation of Energy Savings from Community Scale Solar Water Heating in Los Angeles County

California Energy Commission

Edmund G. Brown Jr., Governor

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PREFACE

The California Energy Commission's Energy Research and Development Division supports energy research and development programs to spur innovation in energy efficiency, renewable energy and advanced clean generation, energy-related environmental protection, energy transmission and distribution and transportation.

In 2012, the Electric Program Investment Charge (EPIC) was established by the California Public Utilities Commission to fund public investments in research to create and advance new energy solution, foster regional innovation and bring ideas from the lab to the marketplace. The California Energy Commission and the state's three largest investor-owned utilities - Pacific Gas and Electric Company, San Diego Gas & Electric Company and Southern California Edison Company - were selected to administer the EPIC funds and advance novel technologies, tools, and strategies that provide benefits to their electric ratepayers.

The Energy Commission is committed to ensuring public participation in its research and development programs that promote greater reliability, lower costs, and increase safety for the California electric ratepayer and include:

- Providing societal benefits.
- Reducing greenhouse gas emission in the electricity sector at the lowest possible cost.
- Supporting California's loading order to meet energy needs first with energy efficiency and demand response, next with renewable energy (distributed generation and utility scale), and finally with clean, conventional electricity supply.
- Supporting low-emission vehicles and transportation.
- Providing economic development.
- Using ratepayer funds efficiently.

Estimation of Energy Savings from Community Scale Solar Water Heating in Los Angeles County is the final report for the community scale solar water heating project GFO-16-502 conducted by the California Center for Sustainable Communities. The information from this project contributes to Energy Research and Development Division's EPIC Program.

All figures and tables are the work of the author(s) for this project unless otherwise cited or credited.

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ABSTRACT

Estimation of Energy Savings from Community Scale Solar Water Heating in Los Angeles County explores the extent to which community scale solar water heating systems, designed for residential structures in Los Angeles County and constructed from currently available technology, can displace natural gas for domestic water heating through a series of case studies. The effects of policy, urban form, and building characteristics on the performance of solar water heating systems, as well as community scale solar water heating's potential to reduce emissions from the residential housing sector, are discussed herein.

Three public and three private residential developments were selected as case studies for community scale solar water heating. These six cases were drawn from the pool of approximately 19,000 "energy communities" in Los Angeles County, i.e. residential developments where the installation and operation of community scale solar water heating systems is broadly feasible. The six properties were also chosen to represent a cross-section housing stock and development patterns common in Los Angeles County, and different levels of suitability for solar water heating. The performance of and energy savings from solar water heating systems on each of these properties is then evaluated using the National Renewable Energy Laboratory's System Advisor Model (NREL SAM). The results of the system simulations reveal how building characteristics and hot water demand affect the performance of community scale solar water heating systems.

The case study site's system simulations show that residential developments with community scale solar water heating can reach site-wide solar fractions of 20-80%, depending on the characteristics of the site's residential buildings and their inhabitants. While the results of the case studies indicate that community scale solar water heating is viable as an emissions reduction technology, side-by-side comparison with other water heating technologies is necessary to determine optimality.

Keywords: *solar water heating, community scale energy systems, water heating, residential energy use*

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EXECUTIVE SUMMARY

Introduction

Reducing greenhouse gas emissions from residential housing is an especially difficult task for California's state and local governments. Demand for electrical and thermal energy varies enormously between consumers, as do the desire and ability to adopt energy efficiency measures and renewable energy technologies. Also, unlike with industrial and commercial consumers, there is little precedent (or appetite) for the government to invasively regulate personal energy consumption. This is especially true of our use of natural gas to heat our homes and water. Whether one decides to cook for themselves or dine out; whether one decides to adjust the thermostat on a cold evening in early November; whether one lingers in the shower for an extra 5 minutes before heading to work – personal energy consumption, especially that of thermal energy, is broadly considered to be the individual's prerogative. However, this freedom and comfort is not without its costs. Water heating alone represents a quarter of California's household energy consumption, and the vast majority of this energy currently comes from natural gas. For this residential water heating, substituting away from natural gas can yield considerable energy savings and emissions reductions, but any policy package designed to encourage an energy transition must contend with the interplay of private expectations, the public good, and the characteristics of the available water heating technologies.

In California, natural gas became the preferred fuel for water heating only after the construction of gas delivery infrastructure and the development of safe, reliable heaters. Currently, more than 90% residences are equipped with natural gas water heaters, but prior to the 1930s, the price and limited availability of gas and abundant sunshine made residential solar water heating systems a very popular alternative for residential water heating.¹ In 1897, one-third of homes in Pasadena had solar water heaters.² In the next several decades thousands of additional units were installed throughout Southern California.^{3,4} Consumers could heat water year-round without having to use a stove, saving fuel and keeping residences cooler during the summer months.⁵ However, falling natural gas prices, urbanization, and incentives for consumers to switch to natural gas eventually led to the displacement of solar thermal

¹ Florida Solar Energy Center. (2006). Solar Water and Pool Heating Manual. *Solar Water and Pool Heating Manual*, (January). Retrieved from <http://www.fsec.ucf.edu>

² Islam, M. R., Sumathy, K., & Khan, S. U. (2012). Solar water heating systems and their market trends. <https://doi.org/10.1016/j.rser.2012.09.011>

³ Denholm, P. (2007). The Technical Potential of Solar Water Heating to Reduce Fossil Fuel Use and Greenhouse Gas Emissions in the United States the Technical Potential of Solar Water Heating to Reduce Fossil Fuel Use and Greenhouse Gas Emissions in the United States, (March), 21. <https://doi.org/NREL/TP-640-41157>

⁴ Islam, M. R., Sumathy, K., & Khan, S. U. (2012). Solar water heating systems and their market trends. <https://doi.org/10.1016/j.rser.2012.09.011>

⁵ Florida Solar Energy Center. (2006). Solar Water and Pool Heating Manual. *Solar Water and Pool Heating Manual*, (January). Retrieved from <http://www.fsec.ucf.edu>

technology from the domestic market.⁶ Fluctuations in energy prices during the 1970s and 1980s led to modest, temporary increases in demand for solar thermal systems, but as of 2009 approximately 91% of households in California have gas water heaters installed.⁷

While subsequent improvements in solar thermal system design methods and component technologies (solar collectors, storage tanks, control units, etc.) have made it possible to build systems that can displace a considerable fraction (>50%) of the natural gas required to meet the hot water demand of a given residential structure, the low price of natural gas means that solar thermal is still one but one potential technological approach for reducing of residential energy consumption and GHG emissions among others.⁸

Project Purpose

This study examines the potential of community scale solar water heating systems to reduce natural gas consumption in Los Angeles County. In this context, “community-scale” describes both the size of the system and an adherence to a set of system design principles. Community scale systems occupy an intermediate space between the domestic and utility scales. This report defines community scale systems as those able to meet the hot water demands of tens of residential buildings up to hundreds of residential units with a solar fraction greater than the minimum required by law.

Community scale energy systems are intended to make maximally efficient use of local resources where possible and create a range of options for residents to contribute to its operation. According to the CEC and National Renewable Energy Laboratory (NREL), community scale solar energy projects should include the following considerations.^{9, 10}

- Primary Considerations
 - Make economically optimum use of local space and resources when and where possible.
 - Develop community scale energy infrastructure in a socioeconomically equitable manner.
- Secondary Considerations
 - Improved economies of sale
 - Improved project siting
 - Exploration of new models for service delivery and project financing.

A community scale approach to solar water heating in LA County is consonant with the considerations listed above. LA County has a mild, Mediterranean climate with abundant sunshine, and the County’s land use and development patterns range from densely populated

⁶ *Ibid.*

⁷ 2009 California Residential Appliance Saturation Study, KEMA Inc.

⁸ Shukla, R., Sumathy, K., Erickson, P., & Gong, J. (2013). Recent advances in the solar water heating systems: A review. *Renewable and Sustainable Energy Reviews*, 19, 173-190.

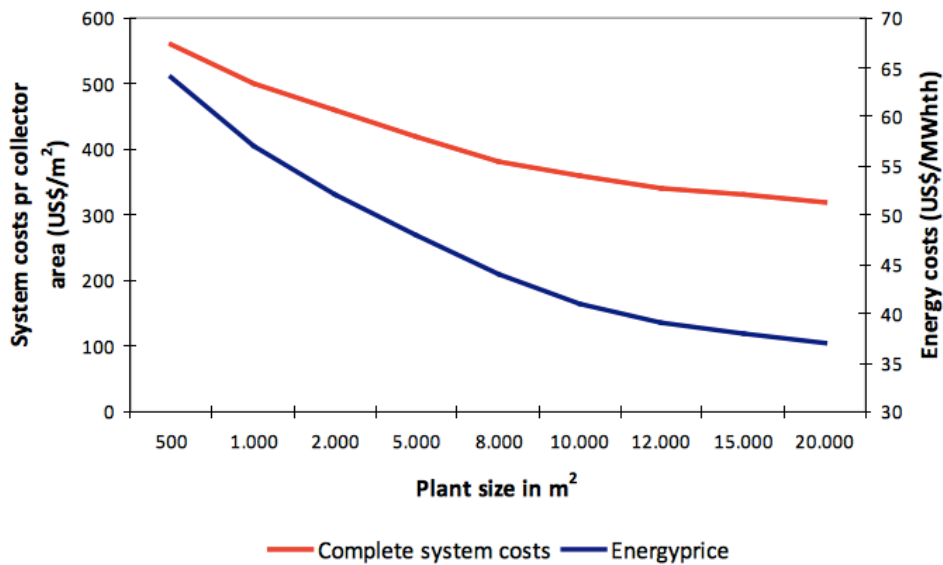
⁹ U.S. National Renewable Energy Lab. (2010). *A Guide to Community Solar: Utility, Private, and Non-profit Project Development*. Retrieved from: <https://www.nrel.gov/docs/fy11osti/49930.pdf>

¹⁰ California Energy Commission. (2017). *Renewable Energy Secure Communities*. Retrieved from: <http://www.energy.ca.gov/research/renewable/community.html>

urban areas to near-rural exurbs. In places where residents cannot afford to install separate domestic systems, or where space for system infrastructure is limited, a community scale approach offers opportunities for all participants to receive the benefits of solar water heating and support a system's operation. Residents may contribute to a system's continued operation by allowing system infrastructure to be installed on their property, or by contributing financially if they do not own property on which system infrastructure can be placed.

Studies of solar district heating in Northern Europe and elsewhere suggest that there are positive returns to scale for solar water heating systems. Large-scale solar thermal systems have shown that both the cost per unit heat delivered and system cost per collector diminish as the total collector area of a district solar heating plant increases.

Figure I. Energy cost and system cost per collector vs. collector area for district solar heating systems.



Source: U.S. Army Corps of Engineers. (2011). *Central Solar Water Heating Systems Design Guide*. Retrieved from: <http://www.solarthermalworld.org/sites/gstec/files/presentation%20Central%20Solar%20Hot%20Water%20Systems.pdf>

A community scale approach to solar water heating may be superior in terms of economic efficiency to the installation of many smaller domestic solar water heating systems. The proportion of the heat load supplied by solar energy, called the *solar fraction* of a system, depends on the amount of useful heat collected and the thermal losses from various system components.¹¹ Larger systems require larger storage tanks, which store heat more efficiently than numerous smaller tanks, thus diminishing the cost per unit heat delivered.¹² Furthermore, community scale systems distribute fixed costs among many users, allowing residents who do

¹¹ Duffie, J. A., & Beckman, W. A. (2013). *Solar engineering of thermal processes*. John Wiley & Sons.

¹² *Ibid.*

not have the financial resources to install their own solar water heating systems to enjoy low carbon hot water and reduce their consumption of natural gas.¹³

Reducing residential natural gas consumption will in turn reduce greenhouse gas emissions, diminish concentrations of local air pollutants (such as SO₂ and NO_x), and mitigate the likelihood of major fires and natural gas leaks.

Given the share of natural gas deliveries consumed to heat water, the end use is an attractive target for reducing the greenhouse gas emissions from the residential housing sector. Residential natural gas consumption represents approximately one-fifth of all natural gas deliveries statewide, and a water heating consumes half of all residential gas deliveries.¹⁴ Water heating accounts for around 25% of total energy end use in residential buildings, and accounts for around 49% of residential natural gas consumption^{15, 16}. In 2016, California’s residential gas consumption for water heating totaled 201,795 million cubic feet, resulting in the emission of eleven million tons of CO₂.¹⁷ This volume of carbon dioxide is equal to that emitted annually by an American city with a population ~700,000.¹⁸ Since water heating accounts for 25% of residential energy consumption, substituting towards renewable sources of thermal energy may yield considerable energy savings for California.

Table I: Natural Gas Deliveries by Consumption Category 1997-2016 (MM ft³)

Consumption Category	Volume of Natural Gas Delivered (MMft ³)	Percentage of Total Gas Deliveries
Residential	9,763,279	21.63%
Commercial	4,915,750	10.89%
Industrial	14,929,914	33.08%
Vehicle Fuel	184,247	0.41%
Electric Power	15,340,675	33.99%

¹³ Del Chiaro, B. & Telleen-Lawton, T. (2007). *Solar Water Heating: How California Can Reduce Its Dependence on Natural Gas*. Environment California Research & Policy Center. Retrieved from: https://www.arb.ca.gov/cc/ccea/comments/jan/environment_california_solar_water_heating.pdf

¹⁴ U.S. Energy Information Administration. (2017). *California Natural Gas Consumption by End Use 1997-2016 [Data set]*. Retrieved from: https://www.eia.gov/dnav/ng/ng_cons_sum_dcu_SCA_a.htm

¹⁵ U.S. Energy Information Administration. (2009). *2009 Residential Energy Consumption Survey [Data set]*. Retrieved from: <https://www.eia.gov/consumption/residential/data/2009/index.php?view=microdata>

¹⁶ Denholm, P. (2007). The Technical Potential of Solar Water Heating to Reduce Fossil Fuel Use and Greenhouse Gas Emissions in the United States The Technical Potential of Solar Water Heating to Reduce Fossil Fuel Use and Greenhouse Gas Emissions in the United States, (March), 21. <https://doi.org/NREL/TP-640-41157>

¹⁷ U.S. Energy Information Administration. (2017). *California Natural Gas Consumption by End Use 1997-2016 [Data set]*. Retrieved from: https://www.eia.gov/dnav/ng/ng_cons_sum_dcu_SCA_a.htm

¹⁸ European Commission Joint Research Centre - EDGAR. (2017). *CO2 time series 1991-2015 per capita for world countries [Data Set]*. Retrieved from: http://edgar.jrc.ec.europa.eu/overview.php?v=CO2ts_pc1990-2015

Total Deliveries	45,133,865	100.00%
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Reducing residential natural gas consumption will also reduce the probability and severity of a catastrophic failure of LA County’s gas delivery and storage infrastructure. Accidental releases of methane, both large and small, decrease California’s emissions budget and make achieving its climate goals more difficult. The 2015 Aliso Canyon Gas Leak alone released 5 billion cubic feet of methane in 112 days. The warming effect of the leak was equivalent to the annual emissions of ~600,000 cars.¹⁹ The storing and transporting large volumes of natural gas inevitably leads to releases, weakening mitigation efforts and worsening climate change.

In addition to the environmental costs of leakages, a large earthquake in Los Angeles County could ignite numerous gas-fueled fires. A study by the California Seismic Safety Commission estimated that 20-50% of fires resulting from a major earthquake ($M > 6.0$) will be caused by the ignition of natural gas leaks.²⁰ Reducing residential demand for natural gas will reduce the volume of gas that must be stored and delivered, mitigating the risk of leakages and fires.

Finally, reducing natural gas consumption will yield public health benefits. The combustion of natural gas produces fewer co-pollutants (such as sulfur or mercury) than the burning of other fossil fuels, but it is still a source of NO_x , CO, and other by-products linked to respiratory and cardiovascular illnesses.²¹ Burning less natural gas reduces local air pollution and the associated mortality risk. Residential use of natural gas also carries with it the risk of carbon monoxide (CO) poisoning. Improperly ventilated or malfunctioning water and space heating devices can cause lethal levels of carbon monoxide to accumulate in enclosed spaces. From 1999-2010, non-fire related CO fatalities occurred at a rate of 430 per year in the US.²² Men and women over the age of 65 are most likely to die from CO poisoning (0.42 and 0.18 deaths per 100,000 people, respectively).²³

Given the environmental and public health costs associated with the use of natural gas, the benefits of substituting towards a renewable source of energy for residential water heating are clear. This study explores what role a community scale solar water heating can play in that transition, taking LA County as a geographic, policy, and climatic context. The cases studies included provide information about the various technologies available for community scale solar thermal systems, the feasibility of community scale water heating, and estimates of

¹⁹ Michanowicz, D. R., Buonocore, J. J., Rowland, S. T., Konschnik, K. E., Goho, S. A., & Bernstein, A. S. (2017). A national assessment of underground natural gas storage: identifying wells with designs likely

²⁰ California Seismic Safety Commission. (2002). *Improving Natural Gas Safety in Earthquakes*. Retrieved from: <http://www.seismic.ca.gov/pub/Final%20CSSCGasSafetyReport%20w%20Figures%207-15-02%20Version.pdf>

²¹ Haines, A., McMichael, A. J., Smith, K. R., Roberts, I., Woodcock, J., Markandya, A., Wilkinson, P. (2009). Health and Climate Change 6 Public health benefits of strategies to reduce greenhouse-gas emissions: overview and implications for policy makers. *The Lancet*, 374, 2104-2114. <https://doi.org/10.1016/S0140>

²² Centers for Disease Control and Prevention. (2014). *QuickStats: Average Annual Number of Deaths and Death Rates from Unintentional, Non-fire Related Carbon Monoxide Poisoning by Sex and Age Group - United States, 1999-2010*. Retrieved from: <https://www.cdc.gov/mmwr/preview/mmwrhtml/mm6303a6.htm>

²³ Ibid.

energy savings generated community scale solar water heating systems. The influence of urban form and building code on the performance of community scale systems is also discussed.

Project Process

Evaluating the energy-saving potential of community scale solar water heating proceeded in four steps: the design of a general-purpose, scalable solar water heating system to serve as the basis for community scale solar water heating system simulations, the selection of simulation methods and case study sites, the running of simulations and analysis of their results.

Selection of Component Technologies & System Design

Unlike solar photovoltaic systems, there are several varieties of solar thermal collector and heat storage technology. Their use depends on the details of the desired application. In order to evaluate the energy savings of community scale solar water heating systems, it was necessary to select from among the available component technologies and create a prototypical system whose behavior could be simulated using computational methods. The prototypical system was designed with guidance from engineers who construct and operate solar thermal systems, and complies with state and local building code requirements.

Development of Project Methodology

Once a satisfactory prototypical solar water heating system was specified, it was then necessary to determine the best methods for simulating the operation of community scale solar water heating systems and determining the values of simulation inputs, chief among them being hot water demand. Input from the project's TAC was invaluable for accomplishing these tasks. It was determined that the National Renewable Energy Laboratory's System Advisor Model's solar water heating module was best given the focus and requirements of the study. The volume of hot water consumed on a daily basis was calculated using series of technical assumptions from the American Society of Heating, Refrigerating, and Air-Conditioning Engineers and the American Society of Plumbing Engineers.

Selection of Case Study Sites

After the design of prototypical community scale system and the selection of a simulation methods, the next task was to select a set of six residential properties in LA County for which simulations of community scale solar water heating systems would be run. This task involved the creation of a set of basic feasibility criteria and a metric to measure the suitability of a given property for a community scale approach to solar water heating. The cases are intended to reflect a range of different urban forms and property ownership arrangements.

System Simulations and Analysis of Results

Following the selection of the six case study sites from the ~19,000 potential sites, data on the sites' buildings, the demographics of the residents, the legal statuses of the site's owners/managers was collected. A characteristic daily demand schedule for hot water and the implied consumption of natural gas was constructed for each site based on the information collected. Simulations for the 102 buildings on the six sites were run, and their results analyzed.

Project Results

The case studies and simulation results show that community scale solar water heating is, given the current policy and economic context, feasible for residential developments ranging in size from small multifamily structures to large, multi-structure housing complexes. The solar fractions of the systems simulated ranged between 20-80%, indicating that community scale systems are capable, under the right conditions, of generating considerable energy savings. Solar water heating systems that met California Title 24 and incentive program requirements were designed using basic system sizing guidelines in all but one case, where an exception had to be made to meet the minimum solar fraction required under Title 24.

Interviews conducted with property owners, solar contractors, engineers and others illustrated the difficulty in programmatically estimating the cost of installing solar thermal systems. Unlike photovoltaic systems, the cost of a solar thermal retrofit depends on the condition and configuration of a building's plumbing, and whether the natural gas heaters that are currently installed can be used as auxiliary heaters. Engineers, owners, and contractors also stressed that qualification for incentives is essential for any solar water heating project (single family or community scale) to be economically and practically feasible.

Finally, the case studies and simulation results made possible a detailed discussion of how the available solar thermal heating incentives affect the decision landscapes faced by different types of property owners (private/ private nonprofit/ public) vis-à-vis solar water heating. A detailed review of the incentive programs and information gathered in interviews shows that it is easiest for private property owners claim the available solar thermal incentives, and thus retrofit their properties for community scale solar water heating.

Benefits to California

As mentioned previously, community scale solar water heating is one technological tool for reducing the residential housing sector's consumption of natural gas among many. Electrification, heat pump-PV systems, biomass, and other thermal generation and cogeneration technologies are also potential sources of low-carbon thermal energy for residential use. Determining the set of applications for which a particular thermal energy technology is best suited is an essential first step in designing policy to encourage or mandate its adoption.

Pursuant to that end, this research project summarizes the policy environment in Los Angeles County with regard to solar water heating (system design requirements, incentive programs and their requirements) and current engineering practices from solar engineering firms operating in the County. The prototypical solar thermal system that emerged from this process can be used in future research projects, such as economic studies of solar thermal systems, and comparisons between alternative renewable heating technologies.

This research partially accomplishes the task of describing the set of residential properties that are best served by community scale solar water heating in Los Angeles County. It provides feasibility criteria that can be used to find sets of parcels where a community scale approach to solar water heating is possible, but additional performance data from more detailed simulations is necessary for validation.

The results of the simulations show that the prototypical solar water heating system, for the properties selected, provide between 20-80% of the energy required for water heating. This study's methods can be altered and scaled to provide regional estimates of the energy savings from the adoption of community scale solar water heating.

CHAPTER 1:

Selection of Solar Water Heating Technologies

The fundamental elements of solar water heating systems include solar thermal collectors, storage tanks (to store the heated working fluid/ heated water), and piping systems to move heated water and working fluid between collectors, storage tanks, and buildings. Additional elements may include heat exchangers, auxiliary gas heaters, buffer tanks, etc.. Control mechanisms for solar water heating systems depend on a given system's size and complexity.²⁴ Chapter 1 explains how the prototypical system for community scale solar water heating emerged from a review of the available solar thermal technologies and input from local contractors and engineers.

1.1 Solar Thermal Collectors

Solar thermal collectors absorb thermal energy from incident solar radiation, and transfer to water or a working fluid. The four most common collector types are:

- Flat Plate Collectors (FPCs)
- Evacuated Tube Collectors (ETCs)
- Integrated Photovoltaic/ Thermal (PV/T) Collectors

Selection of a collector type depends on the desired application and cost. The amount of useful heat a collector delivers to a given system is a function of the amount of incident solar radiation, the difference between ambient temperature and that of the unit, and the temperature of the heat transfer fluid at the collector inlet.²⁵ Collector performance is also affected by the angle of insulation and local meteorological conditions.²⁶ Table 1 lists the peak thermal efficiencies for different collector types measured in laboratory settings

²⁴ Fisch, M. N., Guigas, M., & Dalenbäck, J.-O. (1998). A review of large-scale solar heating systems in Europe. *Solar Energy*, 63(6), 355-366. [https://doi.org/10.1016/S0038-092X\(98\)00103-0](https://doi.org/10.1016/S0038-092X(98)00103-0)

²⁵ Duffie, J. A., & Beckman, W. A. (2013). *Solar engineering of thermal processes*. John Wiley & Sons.

²⁶ *Ibid.*

Table 1: Thermal Efficiency Ranges of Solar Collector Technologies

Collector Type	Peak Thermal Efficiency ($T_i=T_a$)
Flat Plate	70-80% ^{27, 28}
Evacuated Tube	~60% ²⁹
PV/T	50-70% ³⁰
Integrated Collector Storage	Variable ³¹

Peak thermal efficiencies show here are based on laboratory studies measuring useful heat output obtained from a fixed amount of incident radiation and an ambient temperature equal to collector inlet temperature ($T_i = T_a$).

1.1.1 Flat Plate Collectors (FPCs)

A flat plate collector is an insulated box containing an absorber plate and a network of flow tubes covered by a sheet of translucent glass or plastic. Most FPCs have copper flow tubes and absorber plates with selective coatings to reduce reflection.³²

FPCs transfer heat to water or a working fluid as it passes through the network of flow tubes in thermal contact with the absorber plate. The translucent cover serves to reduce heat losses from convection. Figure 1 shows a typical FPC design.

²⁷ Zondag, H. A. (2008). Flat-plate PV-Thermal collectors and systems: A review. *Renewable and Sustainable Energy Reviews*. <https://doi.org/10.1016/j.rser.2005.12.012>

²⁸ Ayompe, L. M., Duffy, A., Mc Keever, M., Conlon, M., & McCormack, S. J. (2011). Comparative field performance study of flat plate and heat pipe evacuated tube collectors (ETCs) for domestic water heating systems in a temperate climate. <https://doi.org/10.1016/j.energy.2011.03.034>

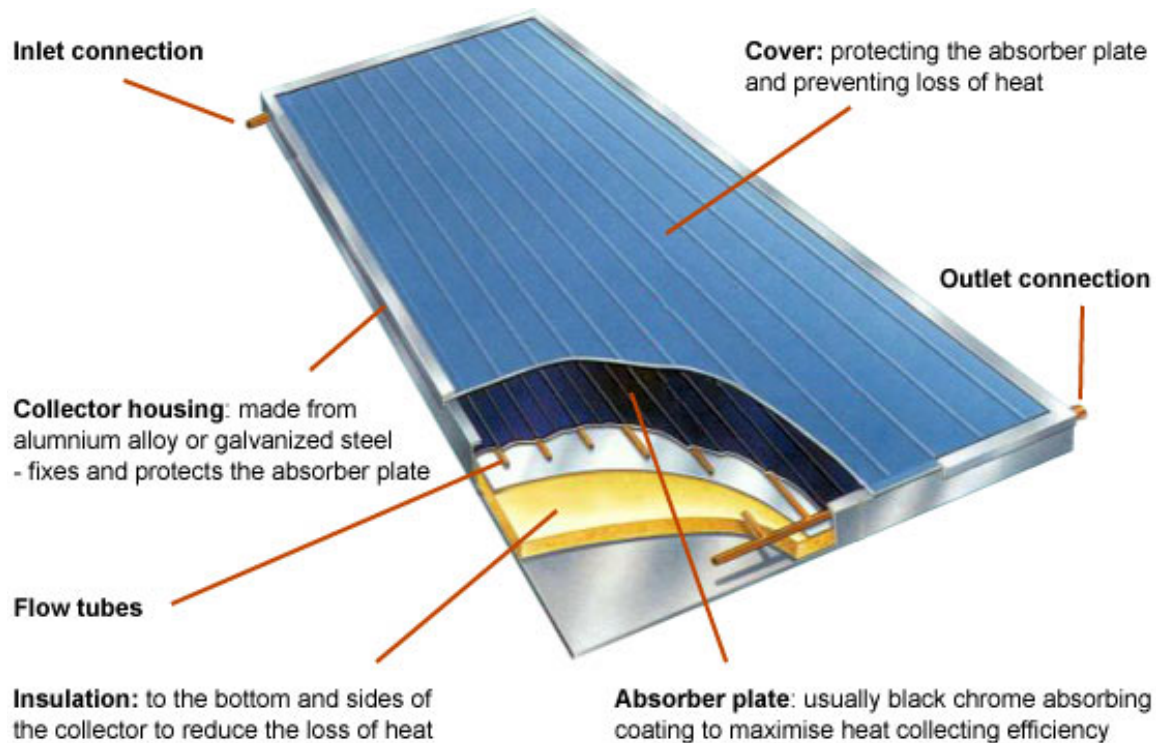
²⁹ *Ibid.*

³⁰ Dubey, S., & Tiwari, G. N. (2008). Thermal modeling of a combined system of photovoltaic thermal (PV/T) solar water heater. *Solar Energy*. <https://doi.org/10.1016/j.solener.2008.02.005>

³¹ Smyth, M., Eames, P. C., & Norton, B. (2006). Integrated collector storage solar water heaters. *Renewable and Sustainable Energy Reviews*, 10(6), 503–538. <https://doi.org/10.1016/j.rser.2004.11.001>

³² Duffie, J. A., & Beckman, W. A. (2013). *Solar engineering of thermal processes*. John Wiley & Sons.

Figure 4: Flat Plate Solar Collector



Source: <https://www.designingbuildings.co.uk>

In controlled settings, flat plate collectors exhibit thermal efficiencies of approximately 75%.³³ This should be considered an upper limit on the thermal efficiency, as the relatively low thermal mass of most flat plate collectors means their performance is sensitive to changes in ambient temperature.^{34,35} The Drake's Landing Solar Community Project, which uses an array of 800 flat plate panels to heat 52 single family homes, has documented a thermal efficiency range for the collection system (collectors and pipes) between 30-70%, with an average of approximately 50%.³⁶

³³ Zambolin, E., & Del Col, D. (2010). Experimental analysis of thermal performance of flat plate and evacuated tube solar collectors in stationary standard and daily conditions. *Solar Energy*, 84(8), 1382-1396.

³⁴ *Ibid.*

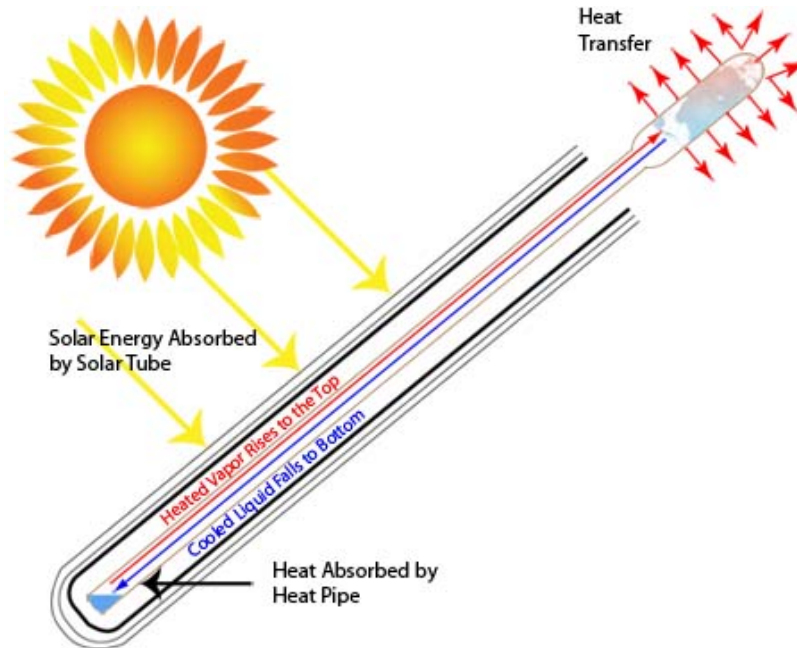
³⁵ *Ibid.*

³⁶ Sibbitt, B., McClenahan, D., Djebbar, R., Thornton, J., Wong, B., Carriere, J., & Kokko, J. (2012). The performance of a high solar fraction seasonal storage district heating system - Five years of operation. *Energy Procedia*, 30, 856-865. <https://doi.org/10.1016/j.egypro.2012.11.097>

1.1.2 Evacuated Tube Collectors

Evacuated tube collectors consist of an array of evacuated glass tubes, each containing a smaller glass tube within. The inner glass tube houses an absorber plate in thermal contact with a flow tube. A vacuum between the two glass layers serves to thermally insulate the inner tube.

Figure 2: Evacuated Tube Solar Collector



Source: <https://www.designingbuildings.co.uk>

There are two main types of evacuated tube collector designs, but all designs employ absorptive coatings on the surface of either the inner tube wall or the absorber plate. Some evacuated tube collector designs include heat pipes that terminate in heat bulbs, around which water flows through a heat exchange manifold. Alternatively, direct circulation designs circulate a working fluid through u-shaped pipes within each of the inner tubes, and return the heated fluid to a header pipe.

A comparison of flat plate and direct circulation evacuated tube collectors' thermal efficiencies found that evacuated tube collectors have slightly lower peak thermal efficiencies than flat plate collectors (<60%), but are less sensitive to changes in ambient temperature and the direction of incident solar radiation.³⁷ Evacuated tube collectors are more efficient over a greater range of meteorological conditions and temperatures than flat plate designs.³⁸ The superior thermal performance of ETCs in variable weather conditions is also supported by data

³⁷ Zambolin, E., & Del Col, D. (2010). Experimental analysis of thermal performance of flat plate and evacuated tube solar collectors in stationary standard and daily conditions. *Solar Energy*, 84(8), 1382-1396. <https://doi.org/10.1016/j.solener.2010.04.020>

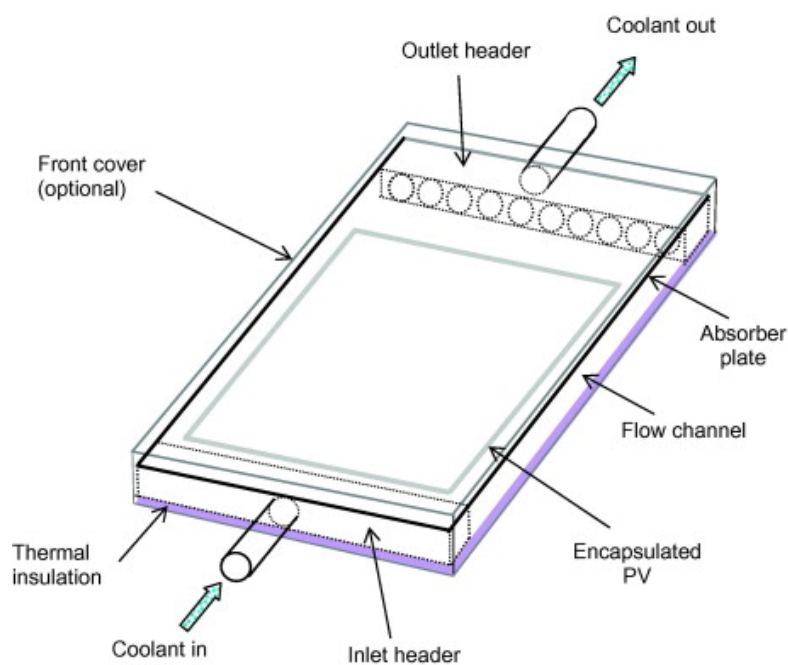
³⁸ Ibid.

from a study domestic solar water heating systems in Dublin, Ireland.³⁹ ETC systems had greater average annual solar fractions (50.3%) than FPC systems (37.9%).⁴⁰

1.1.3 Integrated PV/T Collectors

Integrated PV/T collectors couple the generation of electric current from photovoltaic solar cells with the collection thermal energy for water and space heating. The conversion of solar energy into electric current via the photoelectric effect is a process which is a relatively inefficient process that produces a large amount of waste heat. The collection of waste heat from PV cell arrays both increases the efficiency of the cells themselves (which diminishes as their temperature increases) and provides thermal energy for space and water heating.⁴¹

Figure 3: PV/T Cell



Source: Chow, T. T. (2010). A review on photovoltaic/thermal hybrid solar technology. *Applied Energy*, 87(2), 365–379. <https://doi.org/10.1016/j.apenergy.2009.06.037>

A myriad of PV/T collector designs exist, but all systems involve the circulation a fluid coolant to collect waste heat from photovoltaic cells. PV/T collectors may include a translucent housing or cover to increase thermal absorptivity.⁴² Theoretically, PV/T technology is be the most efficient method for collecting solar energy. High-performing PV/T cells could potentially

³⁹ Ayompe, L. M., Duffy, A., Mc Keever, M., Conlon, M., & McCormack, S. J. (2011). Comparative field performance study of flat plate and heat pipe evacuated tube collectors (ETCs) for domestic water heating systems in a temperate climate. *Energy*, 36(5), 3370-3378.

⁴⁰ *Ibid.*

⁴¹ Huang, B. J., Lin, T. H., Hung, W. C., & Sun, F. S. (2001). Performance evaluation of solar photovoltaic/thermal systems. *Solar Energy*, 70(5), 443-448. [https://doi.org/10.1016/S0038-092X\(00\)00153-5](https://doi.org/10.1016/S0038-092X(00)00153-5)

⁴² *Ibid.*

obviate the need for separate photovoltaic and thermal systems. However, the lower thermal performance of PV/T systems relative to other solar thermal collectors has limited PV/T's adoption.⁴³ PV/T systems collect solar thermal energy indirectly, only about 75% of incident solar energy is available in the form of heat. Maximum thermal efficiencies for PV/T solar collectors range from 50-70%.^{44, 45} Like the other collector technologies discussed previously, thermal efficiencies of PV/T collectors vary depending on ambient temperature, meteorological conditions, and the angle of incident radiation.⁴⁶

1.2 Solar Storage Tanks

The design and use of storage tanks for water and working fluid has a significant impact on the thermal performance of solar water heating systems.⁴⁷ Storage tank insulation and temperature stratification help to minimize thermal losses from solar hot water heating systems. Thermal insulation of tanks helps minimize losses to the ground and air, especially during colder months. Many domestic and community-scale solar water heating systems take advantage of temperature stratification in their designs to increase thermal efficiency.^{48, 49, 50}

Thermal stratification refers to the tendency of hotter, less dense, water to rise to the top of a column. Thermally stratified tanks are designed so as to preserve a temperature gradient along the axis of a storage tank. Hot water may be discharged for consumption from the hottest part of the tank, while water from the coldest part of the tank may be recirculated through the collector array or heat exchanger. Modeling and physical studies of solar hot water heating systems have found that systems employing stratified tanks can deliver approximately 30% more energy than systems that maintain a uniform tank temperature.⁵¹

1.2.1 Auxiliary and Backup Heating Elements

Due to economic and practical considerations, most solar water heating systems are not designed to meet 100% of their heat loads with solar energy.⁵² Instead, systems are designed to

⁴³ Dupeyrat, P., Menezo, C., & Fortuin, S. (2014). Study of the thermal and electrical performances of PVT solar hot water system. *Energy and Buildings*, 68(PART C), 751-755. <https://doi.org/10.1016/j.enbuild.2012.09.032>

⁴⁴ Chow, T. T. (2010). A review on photovoltaic/thermal hybrid solar technology. *Applied Energy*, 87(2), 365-379. <https://doi.org/10.1016/j.apenergy.2009.06.037>

⁴⁵ Dupeyrat, P., Menezo, C., & Fortuin, S. (2014). Study of the thermal and electrical performances of PVT solar hot water system. *Energy and Buildings*, 68(PART C), 751-755. <https://doi.org/10.1016/j.enbuild.2012.09.032>

⁴⁶ Ibid.

⁴⁷ Cruickshank, C. A., & Harrison, S. J. (2010). Heat loss characteristics for a typical solar domestic hot water storage. *Energy and Buildings*, 42(10), 1703-1710. <https://doi.org/10.1016/j.enbuild.2010.04.013>

⁴⁸ Ibid.

⁴⁹ Bauer, D., Marx, R., Nußbicker-Lux, J., Ochs, F., Heidemann, W., & Müller-Steinhagen, H. (2010). German central solar heating plants with seasonal heat storage. *Solar Energy*, 84(4), 612-623. <https://doi.org/10.1016/j.solener.2009.05.013>

⁵⁰ Hollands, K. G. T., & Lightstone, M. F. (1989). A review of low-flow, stratified-tank solar water heating systems. *Solar Energy*, 43(2), 97-105. [https://doi.org/10.1016/0038-092X\(89\)90151-5](https://doi.org/10.1016/0038-092X(89)90151-5)

⁵¹ Ibid.

⁵² Duffie, J. A., & Beckman, W. A. (2013). *Solar engineering of thermal processes*. John Wiley & Sons.

provide hot water at a minimum solar fraction, and use an in-line auxiliary heater to ensure adequate delivery temperature. Auxiliary heaters may also be integrated in to storage tanks, rather than placed in-line with the storage tank outlet pipe. At domestic scales, tank-less water heating units have sufficient power to satisfy demand in the event of insufficient solar radiation or system malfunction.

For systems larger than domestic scale, it may be necessary to include back-up heating units to ensure that hot water can be supplied in the event of inclement weather or malfunction.⁵³ A range of options for back-up heaters exists, including heat pumps, electric and gas heaters, and biomass boilers.⁵⁴ Choice of a particular backup technology is depends on application and cost.

1.2.2 Heat Exchange Fluids and Heat Exchangers

Closed systems with freeze resistant heat exchange fluids are required in climates that experience prolonged freezing temperatures, as most collectors are not designed to withstand such forces. Antifreeze agents are also toxic, requiring a heat exchanger be installed between the collection and storage/ delivery loops.

Common heat exchange fluids include glycol/ water mixtures, hydrocarbon oils, and silicones. Choice of a heat transfer fluid depends on system design and meteorological conditions.⁵⁵

1.3 Solar Thermal System Types

1.3.1 Passive vs. Active Systems

The terms “passive” and “active” describe whether a solar heating system uses energy to circulate water or working fluid through the collector array. Active systems use pumps and powered control elements to circulate water or a working fluid. There are two basic active system designs: direct systems, which circulate potable water through solar thermal collectors, and closed systems, which use a working fluid and heat exchangers to transfer energy to stored water.⁵⁶

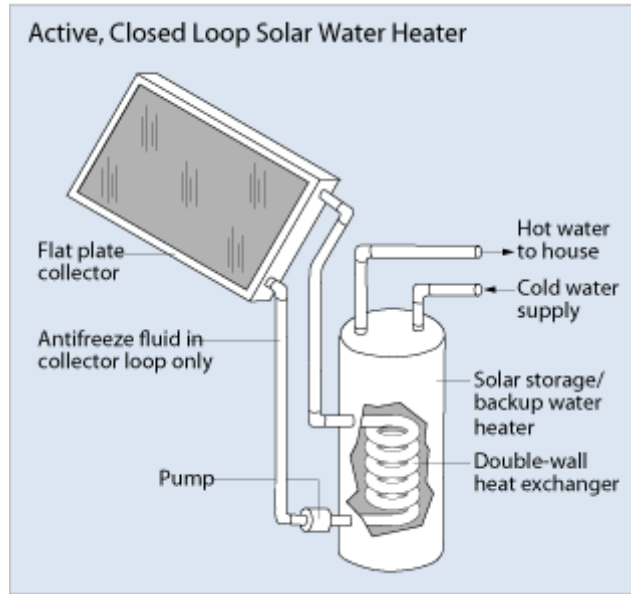
⁵³ Ibid.

⁵⁴ U.S. Army Corps of Engineers. (2011). Central Solar Hot Water Systems Design Guide. Retrieved from: https://www.wbdg.org/FFC/ARMYCOE/COEDG/dg_solar_hot_water.pdf

⁵⁵ U.S. Department of Energy. (2017). Heat Transfer Fluids for Solar Water Heating Systems. Retrieved from: <https://energy.gov/energysaver/heat-transfer-fluids-solar-water-heating-systems>

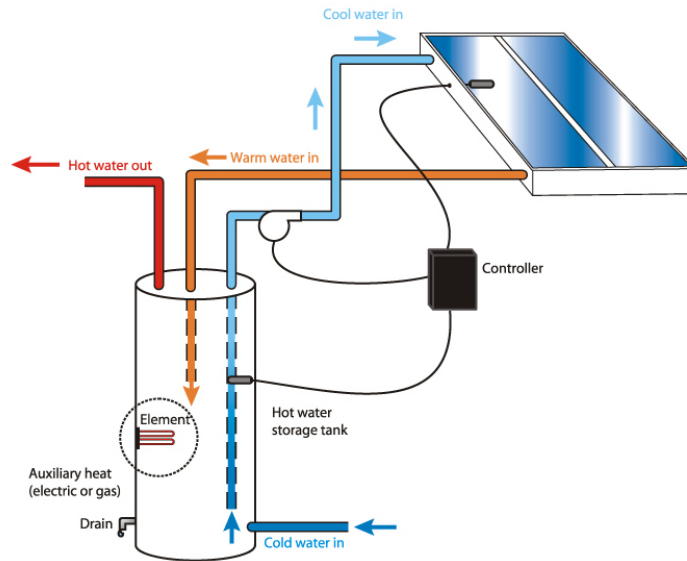
⁵⁶ Ibid.

Figure 4: Schematic of an active closed system



Credit: <https://energy.gov/energysaver/solar-water-heaters>

Figure 5: Schematic of an active, direct system



Credit: http://www.acmegreen.com/page2/page7/files/page7_1.jpg

Community scale solar water heating systems considered in this study will be active systems. Passive systems are most common at the domestic scale. To function properly, passive systems must have collector arrays located below the storage tank, and the storage tank must be installed above the fixtures where hot water is to be used. While passive system designs are potentially sufficient for single residences, they are not practical for larger scales.

1.4 Review of Building and Industry Codes for Community Scale Solar Water Heating

The following section reviews the building and industry codes relevant to the design and construction of community scale solar water heating systems. First, standards for solar water heating system performance and component technologies are reviewed. These standards set minimum requirements for thermal performance and durability, influencing system design and cost.

Secondly, because subsequent analyses will simulate the performance of community-scale solar water heating systems, special attention is paid to regulations governing where system infrastructure may be installed. Rules constraining where and how collector arrays, tanks, etc., are installed will inform the siting of equipment in subsequent case studies.

The design and construction of residential solar water heating systems are most heavily regulated by the state of California and local governments. Both California and Los Angeles County have specific system design and performance requirements that must be met for builders to receive construction permits and for systems to qualify for incentive programs (i.e. CSI Thermal). This section includes a summary of those regulations and explains their influence on community scale system design.

1.4.1 Industry Codes for Community Scale System Components

The Solar Rating and Certification Corporation (SRCC) is a nonprofit organization responsible for the testing and certification of solar thermal technologies in the United States. SRCC is a member of the International Code Council, and its testing requirements are based on the International Standardization Organization's (ISO) codes.

The SRCC has two solar thermal technology rating certifications, OG-100 and OG-300. The OG-100 certification program sets standards for the durability and thermal performance of solar thermal collectors. The OG-300 program applies to single-residence solar water heating systems, and requires that systems meet an overall standard minimum thermal performance.⁵⁷

OG-100 Solar Collector Certification Program

California requires that all domestic and multi-family solar water heating systems use solar thermal collectors approved by the SRCC to be eligible for CSI Thermal renewable energy credits. The SRCC's standards and test sequence for solar collectors are known as the OG-100 Minimum Standards.⁵⁸ OG-100 makes use of ISO 9806 standards. Separate test sequences exist for FPC and ETC collectors.⁵⁹

⁵⁷ International Code Council. (2015). *2015 ICC 900/SRCC 300 - 2015 Solar Thermal System Standard*. Retrieved from: <https://codes.iccsafe.org/public/document/toc/569/>

⁵⁸ International Code Council. (2015). *2015 ICC 901/SRCC 100 2015 Solar Thermal Collector Standard*. Retrieved from: <https://codes.iccsafe.org/public/document/code/570/9961307>

⁵⁹ *Ibid.*

The OG-100 certification process consists of laboratory test sequences for different types of thermal collectors. Solar thermal collectors that meet or exceed testing criteria are listed on the SRCC’s website. Physical specification and thermal performance data are provided for each unit that receives OG-100 certification.

1.4.2 California State Building Code

Below is a summary of the state building codes with the greatest impact on solar water heating system design and siting. Other components of a solar water heating system, such as plumbing systems, control elements are also subject code requirements, but these do not affect basic system design. Code requirements that influence the selection of collection and storage technologies are discussed below.

Title 24, Section 6 – Building Energy Efficiency Standards

A community scale approach to solar water heating will require the installation of systems that serve numerous residential units. Community scale systems thus need to comply with the multi-family solar water heating codes of California’s Title 24. The most fundamental of these requirements is that multi-family systems use SRCC OG-100 certified solar collectors, and that they meet the basic eligibility requirements listed in Table 5.

Multi-family solar water heating systems installed in California are required to meet a minimum average annual solar fraction.⁶⁰ Table 4 summarizes the minimum solar fractions required for each of the California Energy Commission’s (CEC) climate zones. Because the solar fraction of a system varies depending on insolation levels, meteorological conditions, and the precise details of construction and operation, system modeling methods are used to calculate an approximate value for annual solar fraction. This calculated value must meet or exceed the minimum solar fraction for the climate zone. Calculations must be performed with software approved for use by the CEC. Approved programs include both regression and simulation methods for modeling solar water heating system performance.⁶¹

Table 2: Minimum solar fraction by CEC climate zone

Climate Zone	Minimum Solar Fraction
1-9	20%
10-16	35%

Credit: <https://energycodeace.com/site/custom/public/reference-ace-2016/index.html#!Documents/59solarwaterheating.htm>

⁶⁰ California Building Code. (2016). *2016 Building and Appliance Efficiency Regulations*. Retrieved from: <https://energycodeace.com/site/custom/public/reference-ace-2016/index.html#!Documents/59solarwaterheating.htm>

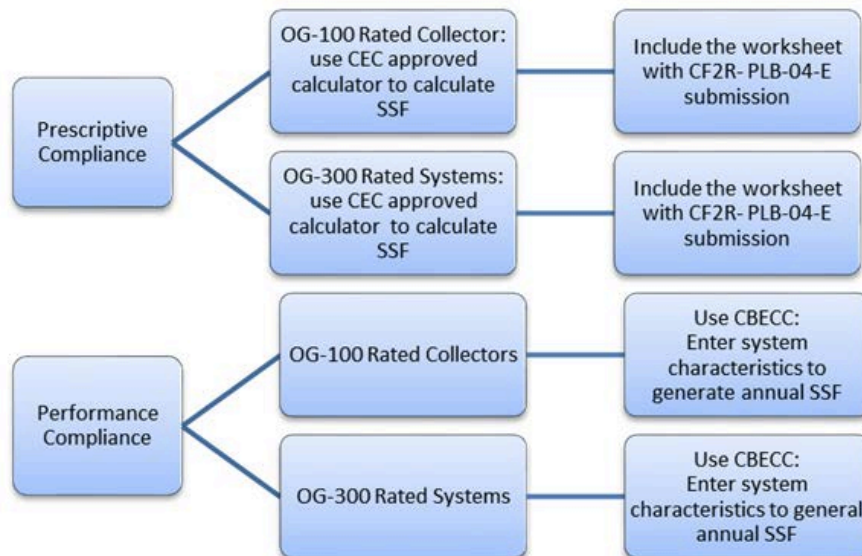
⁶¹ Ferris, T., Froess, L., Meyer, C., Ashuckian, D. (2016). *Residential Alternative Calculation Method Reference Manual*. Retrieved from: http://www.energy.ca.gov/business_meetings/2016_packets/2016-06-14/Item07_ACM%20Ref%20Manuals/2016%20Res%20ACM%20Ref%20Manual%20June%202016.pdf

Table 3: Eligibility criteria for energy efficiency measures – Solar water heating systems (RA4.4.21)

System Certification Type	Eligibility Criteria
SRCC OG-100	(a) Include all features modeled and generated in the CEC approved solar savings fraction calculation
	(b) The collectors should be installed according to manufacturer's instructions
	(c) The collectors shall be located in a position not shaded by adjacent buildings or trees between 9:00AM and 3:00 PM (solar time) on December 21 st .

Figure 6 shows the process flows for prescriptive and performance compliance approaches for solar thermal systems. Selection of an appropriate code compliance approach depends on system scale and design solar fraction. In the case of community scale solar water heating systems intended to reduce the carbon intensity of water heating, a performance approach is most reasonable.

Figure 6: Prescriptive and performance compliance pathways for solar water heating systems



Credit: <https://energycodeace.com/site/custom/public/reference-ace-2016/index.html#!Documents/59solarwaterheating.htm>

A community scale approach to solar water heating requires the installation of collector arrays on multiple residential buildings, including single and multi-family structures. This complicates the task of reaching compliance through a prescriptive approach, as those requirements

assume that residential solar water heating systems only serve a single structure. Therefore, prior to the evaluation of energy savings from community scale solar water heating systems, solar fraction will be estimated via simulation to ensure minimum solar fraction requirements are met.

1.4.3 Los Angeles County Municipal Code

County building permits are required for solar photovoltaic or thermal systems are required prior to construction. The County’s “Guidelines for Plan Check and Permit Requirements for Solar Energy Systems”, effective since 2015, enumerates the municipal requirements relevant to the design and construction of community scale solar water heating systems.⁶² LA County’s guidelines require that solar water heating systems meet state energy efficiency, plumbing, and electrical codes, in addition to complying with zoning restrictions. The Los Angeles County municipal code does not contain specific solar water heating system design requirements beyond those in the state code.⁶³

1.4.4 Incentive Program Eligibility Requirements

Community scale solar water heating systems should take advantage of incentive programs to offset the cost of installation and construction where and when possible. The California Solar Initiative is a subsidy program intended to encourage the proliferation of solar thermal technology for space and water heating.⁶⁴ The program lists specific eligibility requirements for multi-family residential systems and systems, summarized in Table 4.

Table 4: CSI-Thermal Incentive Program Eligibility Requirements

Solar Water Heating System Incentive Category	Eligibility Requirements
Multi-family <250 kWth, Commercial/ Multi-family > 250 kWth	<p>Equipment</p> <ul style="list-style-type: none"> • OG-100 certified collectors • Active, indirect system type • System must include freeze and stagnation protection according to CEC climate zone. • Direct or passive systems are ineligible • Storage tanks must have R12 insulation • Flow meters <p>Installation Requirements</p> <ul style="list-style-type: none"> • Fluid collector square footage area cannot exceed 1.25 times estimated GDP (gallon per day) • Systems with two or more tanks must have a minimum of 1 gallon of storage volume per square foot of collector

⁶² <https://www.ladbs.org/docs/default-source/publications/information-bulletins/general/guidelines-for-plan-check-and-permit-requirements-for-solar-energy-devices-ib-p-gi2014-027.pdf?sfvrsn=26>

⁶³ *Ibid.*

⁶⁴ California Public Utilities Commission. (2017). *California Solar Initiative - Thermal Program Handbook*. Retrieved from: http://www.gosolarcalifornia.ca.gov/documents/CSI-Thermal_Handbook.pdf

- | | |
|--|--|
| | <ul style="list-style-type: none">• Systems with (Collector area/ GPD) > 1.25 must provide justification for sizing.• R2.6 insulation on all exposed or accessible hot water piping. |
|--|--|

1.5 Prototypical System Design for Community Scale Solar Water Heating in Los Angeles County

Specifying a prototypical community system design is necessary to simulate system performance and estimate energy savings. Any community scale system must meet the design criteria specified by the CEC, Title 24, and Los Angeles County. Community scale solar water heating systems should also be eligible for CSI-Thermal rebates to offset capital costs where possible, given the low cost of competing energy sources.

The following sections explain and justify the selection of component technologies and system design elements for community scale systems in LA County. Building code and rebate eligibility requirements, cost, performance, and climactic conditions are all given consideration in the design of community scale systems.

1.5.1 Selection of Community Scale Solar Water Heating System Components

Estimating the energy savings from community scale solar water heating systems requires the selection of appropriate component technologies for the given application and climate. To establish compliance with minimum solar fraction requirements, the following must be specified:

- **Collector Type**
- **Direct/ Indirect System Type**
- **Thermal Energy Storage Type**
- **Auxiliary Heat Source**

Conventional Solar Thermal Collectors vs. PV/T Collectors

Based on the review of commercially available solar thermal collectors, flat-plate and evacuated tube collectors are potentially suitable for community scale solar water heating systems in LA County.

PV/T are not suitable for community scale solar water heating. While PV/T collectors provide an elegant solution to the problem of PV and thermal systems competing for rooftop space, the cost and durability of existing PV/T cell technologies make them unattractive for community scale applications. PV/T panels are less thermally efficient than standard solar thermal collectors, thus a solar water heating system with PV/T panels must have a larger collector area than a purely thermal system to meet an identical heat load.⁶⁵ PV/T collectors are also more

⁶⁵ Dean, J., McNutt, P., Lisell, L., Burch, J., Jones, D., Heinicke, D. (2015). *Photovoltaic-Thermal Technology Demonstration*. NREL. Retrieved from: <https://www.nrel.gov/docs/fy15osti/63474.pdf>

expensive on the basis of dollars per installed unit of collector area than either FPC or ETC technologies.⁶⁶ Table 7 shows a comparison in terms of dollars per square meter.

Table 5: Cost per square meter of installed collector area – PV/T vs. Thermal

Collector Type	\$/ m ²
PV/T	\$531-\$1121 ⁶⁷
FPC or ETC	\$59-\$223 ⁶⁸

With regards to durability, the materials used to construct some PV/T collectors limits their operational temperature to 130-170°F.⁶⁹ PV/T collectors with EVA laminated PV cells may be damaged by prolonged exposure to temperatures at or above 130°F, as EVA thermally degrades above this temperature.⁷⁰ FPCs and ETCs have much higher stagnation temperatures, between 180-210°C and 220-300°C, respectively.⁷¹ Furthermore, SRCC OG-100 Standards require that collectors be able with withstand 1000 hours of stagnation temperature per year without serious performance degradation. Thus, given the cost and accelerated timetable for performance degradation relative to thermal collectors, PV/T collectors will not be used in the community scale solar water heating systems proposed in this effort.

FPC vs. ETC

The choice of collector technology for community scale systems in LA County may be narrowed to FPC or ETC. The choice the optimal collector technology may be made on the basis of climatic conditions and cost.

Climatic conditions in LA County favor FPCs over ETCs. Figure 15 shows steady-state and daily thermal efficiency curves for both evacuated tube and flat-plate collector types. Thermal efficiency is plotted as a function of the difference between ambient and fluid inlet temperature (reduced temperature) normalized by the level of incident radiation. Daily thermal efficiency measurements were made in Padova, Italy. The thermal efficiency of ETC is less sensitive to changes in ambient or inlet temperature, and outperform FPCs when the difference between

⁶⁶ Matuska, T. (2014). ScienceDirect Performance and economic analysis of hybrid PVT collectors in solar DHW system. *Energy Procedia*, 48, 150-156. <https://doi.org/10.1016/j.egypro.2014.02>.

⁶⁷ *Ibid.*

⁶⁸ <https://www.epa.gov/rhc/rhc-multi-unit-housing#Footnotes>

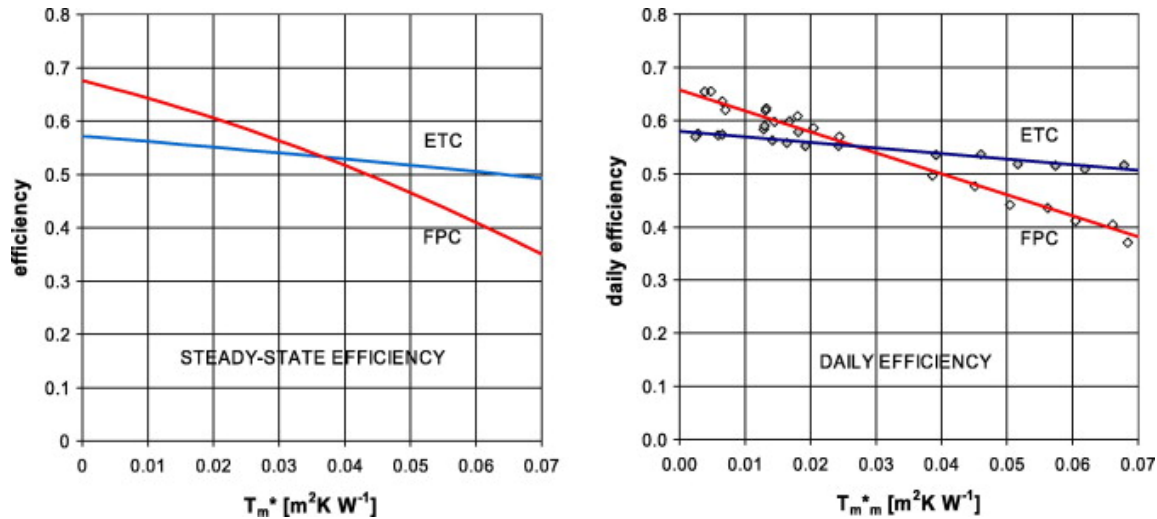
⁶⁹ Zondag, H. A., & Van Helden, W. G. J. (n.d.). *Stagnation Temperature in PVT Collectors*. Retrieved from <http://www.ecn.nl/docs/library/report/2002/rx02045.pdf>

⁷⁰ *Ibid.*

⁷¹ Hausner, R., Fink, C. (2002). *Stagnation Behavior in Solar Thermal Systems*. International Energy Agency – Solar Heating & Cooling Programme. Retrieved from: <http://www.aee-intec.at/0uploads/dateien48.pdf>

ambient and fluid temperatures is large.⁷² However, FPCs are more efficient than ETCs when this difference is small, and when weather conditions are relatively mild.⁷³

Figure 8: Thermal efficiency vs. reduced temperature (T_a-T_i) for FPCs and ETCs under steady-state and field conditions in Padova, It.



Source: Zambolin, E., & Del Col, D. (2010). Experimental analysis of thermal performance of flat plate and evacuated tube solar collectors in stationary standard and daily conditions. *Solar Energy*, 84(8), 1382-1396.

Cost considerations also favor FPCs. FPCs are 20-40% cheaper than ETCs per collector unit, as they are less materially intensive to manufacture.⁷⁴ FPCs will be the default collector type for community scale solar water heating systems in LA County.

Direct/ Indirect System Type

As mentioned previously, direct systems are not eligible for energy credits as per the CSI-Thermal Program Handbook.⁷⁵ Therefore, community scale solar water heating systems will be indirect to take advantage of the available incentives. Community scale systems considered in this analysis may therefore be classified as “indirect forced circulation” systems. Indirect forced circulation systems use pumps to circulate a working fluid within the collector array. Thermal energy is transferred to potable water through a heat exchanger.

Thermal Energy Storage Type

⁷²Zambolin, E., & Del Col, D. (2010). Experimental analysis of thermal performance of flat plate and evacuated tube solar collectors in stationary standard and daily conditions. *Solar Energy*, 84(8), 1382-1396.

⁷³ Ibid.

⁷⁴ Solartown. (2016). *Solar Water Heater Choices: Flat or Evacuated Tube Collectors?*. Retrieved from: <https://solartown.com/learning/solar-water-heaters/solar-water-heater-choices-flat-plate-or-evacuated-tube-collectors/>

⁷⁵ California Public Utilities Commission. (2017). *California Solar Initiative - Thermal Program Handbook*. Retrieved from: http://www.gosolarcalifornia.ca.gov/documents/CSI-Thermal_Handbook.pdf

The volume of thermal energy that a community scale solar thermal systems energy must store, and the duration over which must be stored depends on seasonal variation in the supply of and demand for energy.

Regarding the supply of solar energy, The National Renewable Energy Laboratory (NREL) estimates that Los Angeles County receives enough sunlight for a base case solar water heating system (a single residence with constant load and electric auxiliary heater) to achieve an annual solar fraction >80%.⁷⁶ This suggests that seasonal variation in the intensity and duration of incoming sunlight is not sufficient to warrant the construction of large and expensive seasonal heat stores, and that community scale systems will be able to meet and exceed minimum solar fraction requirements year round, though solar fraction may fluctuate seasonally.

Auxiliary Heat Sources

Community scale solar water heating systems must be able to provide hot water to the residences it serves in the event of extended inclement weather or temporary system shutdown. Solar thermal contractors and heating and cooling engineers use existing natural gas heaters for solar water retrofits when possible to minimize cost.⁷⁷ This practice ensures that hot water is available for a structure's occupants in the event of system malfunction or maintenance. For the purpose of this study, existing natural gas heaters are assumed to function as auxiliary heat sources.

1.5.2 Prototypical System for Community Scale Solar Water Heating

Based on LA County's regulatory environment and climate, a closed, active system with centralized storage of hot water, and a flat-plate collector array is the most suitable configuration for community scale solar water heating systems in Los Angeles County. Such systems are easily scalable, and is the prototypical solar water heating system type considered in this study.⁷⁸

⁷⁶ Cassard, H. Denholm, P., Ong, S. (2011). *Break-even Cost for Residential Solar Water Heating in the United States: Key Drivers and Sensitivities*. NREL. Retrieved from: <https://www.nrel.gov/docs/fy11osti/48986.pdf>

⁷⁷ Bavin, T. (2018 June 7). Personal Communication.

⁷⁸ Chen, W. (2017 Oct. 20). Personal Communication.

CHAPTER 2:

Community Scale Solar Water Heating System Simulation Method

Chapter 2 discusses the methods used estimate putative energy savings from community scale solar water heating systems. Section 2.1 discusses the selection of the simulation method used to estimate system performance and potential energy savings. Section 2.2 explains how hot water demand is estimated using technical assumptions.

2.1 Simulation Methods for Community Scale Solar Water Heating System Performance

Numerous methods exist for the estimation of solar water heating system performance and energy output. Performance calculation methods also vary widely with respect to computational complexity, underlying mathematical structure, assumptions, and flexibility. This study's choice of performance calculation method was determined by the aforementioned considerations, and well as input from the study's Technical Advisory Committee.^{79, 80}

Methods for predicting the performance of solar thermal systems may be classified as either regression or simulation methods.⁸¹ Regression methods correlate the parameters of a given system (collector area, storage volume, fluid flow rates, etc.) with thermal performance using empirical relationships derived from the performance data of existing systems.⁸² The f-Chart Method, approved for the estimation of minimum annual solar fraction under Title 24, is one such method.⁸³ Regression methods are computationally inexpensive compared to simulation methods, and in many instances provide accurate predictions of long term system performance. However, regression methods like the f-Chart are not dynamical. Such methods only predict average performance over a fixed period of time. Thus, a simulation method must be used to model community scale solar water heating system performance.

Simulation methods model the flow of energy and mass through virtual systems at a user-specified time step.⁸⁴ Simulation programs for modeling solar thermal systems differ with respect to their flexibility and complexity; selection of an appropriate simulation program

⁷⁹ Anderson, K. (2017, January 17). Personal Communication.

⁸⁰ Chen, W. (2017, January 17). Personal Communication.

⁸¹ Duffie, J. A., & Beckman, W. A. (2013). *Solar engineering of thermal processes*. John Wiley & Sons.

⁸² *Ibid.*

⁸³ California Energy Commission. (2016). *Title 24 - 2016 Residential Compliance Manual*.

⁸⁴ Lisboa, P., & Fonseca Costa, M. (n.d.). A Software for Performance Simulation of Solar Water Heating Systems. Retrieved from <http://www.wseas.us/e-library/conferences/2012/Istanbul/FLUHE/FLUHE-39.pdf>

depends on the requirements of a particular study. Because this analysis estimates hourly energy output from community scale solar water heating systems using a relatively small set of assumptions about system design and physical parameters, simulation programs with intermediate flexibility and computational complexity are most suitable.

This study uses NREL's System Advisor Model to calculate the hourly energy output from community scale solar water heating systems. The following section describes the simulation assumptions, input parameters, output, and accompanying cost calculations.

2.1.1 NREL System Advisor Model Software

NREL SAM is a free transient energy simulation program developed for modeling renewable energy systems. NREL SAM is used to calculate the daily performance for community scale solar energy systems over the course of one year. NREL SAM uses the implicit Euler method to solve a series of differential equations at each time step. SAM makes two fundamental assumptions about the design of solar water heating systems⁸⁵:

1. Solar water heating systems are indirect. Systems have a closed collection loop through which a working fluid is circulated.
2. Solar water heating systems are active use electric pumps to move fluid through the collector loop.

SAM's output variables for are listed in Appendix A.

2.1.2 Community Scale Solar Water Heating System Siting and Design Considerations

Each case study includes the siting of solar water heating systems on the parcel or parcels of an energy community. Collector arrays, storage tanks, and the pipe lengths must be located in space so that system parameters required for heat loss and other performance calculations may be entered into the System Advisor Model.

Collector Array - Location, Orientation, and Simulation Parameters

Solar thermal collectors will be located on rooftops where possible to minimize shading of collector apertures and within each building rooftop's Solar Zone⁸⁶, as defined in Section 110.10 of California's Title 24.⁸⁷ All structures within an energy community's case study's parcel or parcels are considered as potential sites for collector arrays.

⁸⁵ Burch, J., Christensen, C., DiOrion, N., & Dobos, A. (2014 March 14). *Technical Manual for the SAM Solar Water Heating Model*. National Renewable Energy Laboratory. Retrieved from: https://sam.nrel.gov/system/tdf/SimpleSolarWaterHeatingModel_SAM_0.pdf?file=1&type=node&id=69521

⁸⁶ Definition of Solar Zone for Low Rise and High Rise Multi-Family Buildings: "The Solar Zone shall be located on the roof or overhang of the building or on the roof or overhang of another structure located within 250 ft. of the building or on covered parking installed with the building project. The Solar Zone will have a total area no less than 15% of the total roof area of the building excluding any skylight area"

⁸⁷ California Energy Commission. (2015 June). *2016 Building Energy Efficiency Standards for Residential and Nonresidential Buildings*. Retrieved from: <http://www.energy.ca.gov/2015publications/CEC-400-2015-037/CEC-400-2015-037-CMF.pdf>

NREL SAM contains a library of commercially available glazed flat-plate collectors and performance data derived from testing.⁸⁸ This study will use the SunEarth Empire EP-40 Solar Collector as the prototypical flat plate collector. This collector model is manufactured domestically and is OG-100 certified.⁸⁹ Selection of a collector model from the SAM library automatically specifies the performance parameters listed in the Table 7.

Table 6: SAM Collector Performance Parameters for the SunEarth Empire EP-40 Solar Collector

Parameter	Value
Collector Area	3.8 m ²
FR _{ta} (Hottel-Whillier-Bliss Equation – Optical Gain Coefficient)	0.718
FR _{UL} (Hottel-Whillier-Bliss Equation – Thermal Loss Coefficient)	2.29 W/m ² C
Incidence Angel Modifier Coefficient	0.32
Test Fluid	Glycol
Test Flow	0.076

Solar Storage Tank - Simulation Parameters

Standby losses from solar storage tanks may be minimized by locating them within existing structures.⁹⁰ SAM’s Solar Water Heating model assumes a two tank indirect system with an electric auxiliary heater, with glycol as a heat transfer fluid.⁹¹ These assumptions are consistent with the solar water heating system design details required by state and county regulatory regimes identified in Chapter 1.

SAM requires users specify the ratio of tank height to width. Vertically oriented and thermally stratified tanks increase the performance of solar water heating systems.⁹² This study assumes a height to width ratio of 2:1 for solar thermal and hot water tanks. SAM’s assumes two-node stratification without thermal exchange.⁹³

⁸⁸ Burch, J., Christensen, C., DiOrio, N., & Dobos, A. (2014 March 14). *Technical Manual for the SAM Solar Water Heating Model*. National Renewable Energy Laboratory. Retrieved from: https://sam.nrel.gov/system/tdf/SimpleSolarWaterHeatingModel_SAM_0.pdf?file=1&type=node&id=69521

⁸⁹ SunEarth. (2017). *Empire EP-40 Specification Sheet*. Retrieved from: https://sunearthinc.com/assets/files/EP-40-1.5-10000097_CERT_2012.pdf?r=false

⁹⁰ Duffie, J. A., & Beckman, W. A. (2013). *Solar engineering of thermal processes*. John Wiley & Sons.

⁹¹ NREL. (2011 December 7). *System Advisor Model - Technology Options: Concentrating Solar Power Systems*

⁹² Cruickshank, C. A., & Harrison, S. J. (2010). Heat loss characteristics for a typical solar domestic hot water storage. *Energy and Buildings*, 42(10), 1703-1710. <http://doi.org/10.1016/j.enbuild.2010.04.013>

⁹³ Diorio, N., Christensen, C., Burch, J., & Dobos, A. (2014). *Technical Manual for the SAM Solar Water Heating Model*. Retrieved from https://sam.nrel.gov/system/tdf/SimpleSolarWaterHeatingModel_SAM_0.pdf?file=1&type=node&id=69521

Table 7: Sam Storage Tank Parameters

Parameters	Description
Solar Tank Volume	Volume in cubic meters. Title 24 requires a storage volume to collector area ratio of 1.5 gallons/ 1 ft. ² of collector area.
Solar Tank Height to Diameter Ratio	Tank aspect ratio (2:1)
Solar Tank Heat Loss Coefficient (U-value)	W/ m ² C
Solar Tank Maximum Water Temperature	Maximum allowable temperature in solar tank. Bulk tank temperature cannot exceed this value. Equivalent to the opening of a temperature controlled relief valve.
Outlet Set Temperature	Residential hot water temperature set point (48.89°C)
Mechanical Room Temperature	Used to calculate tank standby loss. $Q_{Loss} = UA_{Tank}(T_{room} - T_{tank})$

In indirect solar water heating systems, heat exchangers transfer thermal energy from the heated working fluid in the solar tank to water for delivery to end users. SAM requires the following parameters to model heat exchange:

Table 8: SAM Heat Exchanger Parameters

Parameter	Description/ Units
Heat Exchanger Effectiveness (e)	$e = (T_{cold-out} - T_{cold-in}) / (T_{hot-in} - T_{cold-in})$

Collection Loop Piping and Pumps - Simulation Parameters

Indirect solar water heating systems have two separate piping systems. One circulates working fluid through the collection array and solar tank, and the other delivers heated water from the auxiliary tank to end users. SAM requires information about the length, diameter, and insulation of the pipes used to collect heat and distribute hot water to residential buildings to calculate heat lost from the collection loop. Collection loop pipe lengths will include the vertical and horizontal distances between collector arrays and solar storage tanks.

SAM assumes that fluid is circulated between the collector array, solar tank, and heat exchangers by an electric pump. The collector pump's peak power rating and efficiency are required to calculate solar fraction and other performance metrics.

Table 9: SAM Pipe and Pump Parameters

Parameters	Description
Total Piping Length in System	Collection Network: Vertical and Horizontal distance between collector arrays (m). Transmission Network: straight line distance plus detours (m).
Pipe Diameter	Average diameter of piping (m)
Pipe insulation Conductivity	W/ m ² C
Pipe Insulation Thickness	Average insulation thickness
Pump Power	Electric pump's peak power rating (W)
Pump Efficiency	Estimated pump efficiency (0 to 1)

Auxiliary Heat Source – Simulation Parameters

All active SWH heating systems have auxiliary heating units to ensure water is delivered at the appropriate temperature. SAM assumes that electric resistance supplies auxiliary heat, and calculates the energy required to raise the temperature of water in the storage tank to the set temperature at each time step. The auxiliary energy required to reach set temperature is given by:

Equation 1: SAM Auxiliary Heat

$$Q_{aux} = m_{draw}c_p(T_{set} - T_{deliv})$$

Where:

Q_{aux} = Auxiliary heat

m_{draw} = Mass of water draw

T_{set} = Set temperature for hot water

T_{deliv} = Temperature of water delivered from solar storage

SAM includes a macro that converts kilowatt-hours of auxiliary electrical energy into volumes of gas using an estimate of the burning efficiency of a typical natural gas heater and a characteristic tank heat loss coefficient. The tank heat loss coefficient depends on a tank's shape and insulation.

Table 10: Parameters for SAM Auxiliary Gas Heater Macro

Parameters	Description
Tank Loss Coefficient	Based on tank insulation value (0-1)
Burning Efficiency	Efficiency of auxiliary natural gas heater (0-100%)

2.2 Hot Water Demand Estimation Methods

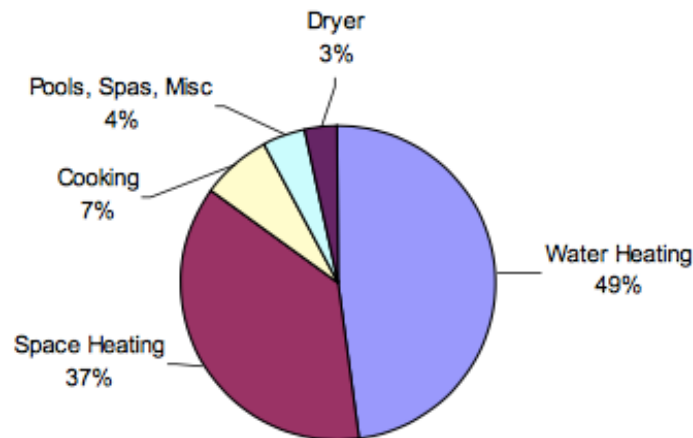
2.2.1 Gas Consumption for Residential Water Heating

The calculation of energy savings requires the estimation of residential gas consumption based on parcel and building-level data. This analysis develops a method to estimate the gas consumed to heat water by residential parcels on a daily basis for one year based on ASHRAE water consumption tables.⁹⁴ Monthly gas consumption data from the Energy Atlas was not used to estimate energy demand due to the inaccuracy inherent in disaggregating gas consumption by end-uses. Daily hot water consumption calculated for the parcels in an energy community will then be used in simulations of community scale SWH system performance.

Limitations of Signal Processing Parcel-level Gas Consumption Data

This study calculates daily hot water demand based on ASHRAE guidelines instead of using consumption data from the Energy Atlas because of the difficulty of disaggregating end-uses from one another. While residential appliance surveys provide estimates of gas consumption for water heating relative to total consumption, there is little data available to help decompose monthly consumption totals into separate end-uses. Patterns of hot water usage and total hot water consumption also vary greatly depending on the demographics of the people who inhabit the structures on a particular residential parcel.⁹⁵

Figure 9: California Residential Gas Consumption by End-use



Source: Palmgren, C., Stevens, N., Goldberg, M., Barnes, R., & Rothkin, K. (2010). 2009 California residential appliance saturation survey.

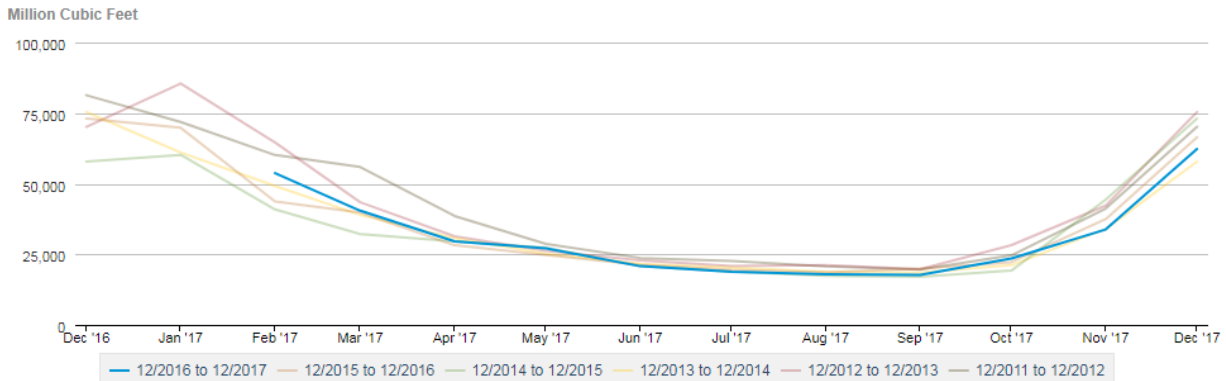
The focus on one end-use among many complicates the estimation of energy savings. It is necessary to remove the contribution of other end uses from to accurately estimate the energy

⁹⁴ Handbook, A.S.H.R.A.E. (2007). Fundamentals. American Society of Heating, Refrigerating and Air Conditioning Engineers, Atlanta, 111.

⁹⁵ Parker, D. S., Fairey, P. W., & Lutz, J. D. (2015). Estimating Daily Domestic Hot- Water Use in North American Homes. ASHRAE Transactions, 121(2). Retrieved from <http://www.ashrae.org>

consumed by water heating. Unfortunately, the structure of the available gas consumption data (monthly billing data for parcels and individual accounts) limits the potential disaggregation to seasonal and non-seasonal end uses. Residential gas consumption in California displays a strong seasonal trend due to the popularity of natural gas for space heating and the state's mild climate.⁹⁶

Figure 10: 10-Year Monthly Residential Gas Consumption (2007-2017)



Source U.S.: Energy Information Administration. (2018). *California Natural Gas Residential Consumption, 1989-2017* [Data Set]. Retrieved from: <https://www.eia.gov/dnav/ng/hist/n3010ca2m.htm>

2.2.2 Hot Water Demand per Residential Unit, and Gas Consumed for Residential Water Heating

Daily hot water demand and the volume of gas required to meet it are calculated for each community scale solar water heating case study. These calculations use data from the LA County Tax Assessor's, sitemaps and maximum occupancy of the residential units at each site, and daily water consumption and water heater efficiency assumptions listed in ASHRAE's *Handbook of Applications*.

Hot Water Demand per Residential Structure

Daily water demand for residential structures are calculated according to Equation 2:

$$\text{Equation 2: Daily Hot Water Demand per Community Parcel}^{97}$$

$$V_{hot} = N_{unit}V_{unit}$$

Where:

V_{hot} = Volume of hot water consumed per residential structure

N_{unit} = Number of residential units per residential structure

V_{unit} = Volume of hot water consumed per residential unit per day

⁹⁶ U.S. Energy Information Administration. (2018). *California Natural Gas Residential Consumption, 1989-2017* [Data Set]. Retrieved from: <https://www.eia.gov/dnav/ng/hist/n3010ca2m.htm>

⁹⁷ Kalogirou, S. A. (2013). *Solar energy engineering: processes and systems*. Academic Press.

The volume of hot water consumed per unit per day (V_{unit}) depends on the number of units in a residential structure.⁹⁸ Values of V_{unit} are estimates of maximum daily hot water consumption in gallons per day (GPD).⁹⁹ The volume of hot water is assumed to be seasonally invariant.

Energy Demand per Residential Structure

The energy demand per parcel per day is then calculated using a parcel's daily volumetric consumption (V_{hot}).

Equation 3: Daily Energy Demand per Community Parcel¹⁰⁰

$$D = V_{hot} \rho c_p (T_w - T_m)$$

Where:

D = Daily energy demand per residential structure

T_w = Delivery temperature of hot water

T_m = Cold water mains temperature

This study assumes a delivery temperature of 120 °F (49 °C). Cold water mains temperature varies seasonally and geographically. A mains temperature profile for Los Angeles is available in NREL SAM.

Equation 4: Daily Natural Gas Consumption per Community Parcel

$$V_{Gas} = \frac{D}{\rho_E} EF_{heater}$$

Where:

V_{Gas} = Daily volume of natural gas consumed for water heating

ρ_E = Energy density of natural gas

EF_{heater} = Energy Factor of the extant water heater

Estimating the energy factor of the extant heater or heaters on a community parcel will require communication with building managers/ property owners. Equation 3 may be modified if electric heaters are installed.

⁹⁸ California Public Utilities Commission. (2017 June). *California Solar Initiative - Thermal Program Handbook*. Retrieved from: http://www.gosolarcalifornia.ca.gov/documents/CSI-Thermal_Handbook.pdf

⁹⁹ Handbook, A. S. H. R. A. E. (2007). Fundamentals. *American Society of Heating, Refrigerating and Air Conditioning Engineers, Atlanta, 111*.

¹⁰⁰ Kalogirou, S. A. (2013). *Solar energy engineering: processes and systems*. Academic Press.

Chapter 3: Case Study Site Selection

Chapter 3 describes how community scale solar water heating case study sites were chosen from broad pools of potential candidate sites. The development of candidate property pools, the selection of case study sites, brief descriptions of the chosen sites are included.

3.1 Practical and Technical Constraints on Community Scale Solar Water Heating

Not all residential parcels are equally suitable for a community scale approach to solar water heating. These constraints include property ownership patterns, transmission losses, available space for collector areas, and ease of permitting. The table below outlines constraint categories.

Table 10: Practical and Technical Constraints for Community Scale Solar Water Heating

Constraints	Issues
Existing Infrastructure	<ul style="list-style-type: none">- Heat Transmission Network- Retrofit vs. New Construction
Technical Limitations	<ul style="list-style-type: none">- Transmission Losses
System and Property Ownership	<ul style="list-style-type: none">- Land Use Patterns- Collective Ownership- Qualification for Incentives- Technical Limitations of Incentives

3.1.1 Existing Infrastructure

The greatest constraint on the development of community scale solar energy systems is the presence and state of existing infrastructure. Regardless of scale or type, all solar energy systems include energy collection and transmission infrastructure.¹⁰¹ Also, virtually all solar energy systems include energy storage to match the supply of thermal or electrical energy with demand. Integration of community scale solar energy systems with existing infrastructure may reduce the cost of construction and operation, and in some cases increase operational scale.¹⁰²

Heat Transmission Network

Currently, there exists no large scale public heat transmission infrastructure in Los Angeles County. The largest central heating system in Los Angeles County belongs to the University of California at Los Angeles and supplies the Ronald Regan Medical Center as well as other

¹⁰¹ Wiseman, H. J., & Bronin, S. C. (2012). Community-Scale Renewable Energy. *San Diego J. Climate & Energy L.*, 4, 165.

¹⁰² *Ibid.*

campus buildings.¹⁰³ Large scale cogeneration and district level heating are more economically feasible in cities with colder climates and denser urban forms, such as New York, San Francisco, and Minneapolis/St. Paul.¹⁰⁴⁻¹⁰⁵⁻¹⁰⁶

Retrofit vs. New Construction

As mentioned in Chapter 1, urban form impacts the feasibility of community scale SWH, and the performance of installed systems. Population density, characteristics of the building stock, and the impact of zoning rules are all potentially influential variables. Thus, in order to produce relevant and realistic estimates of energy savings, this study includes only retrofit case studies. Case studies should be representative of the urban environment in LA County as it currently exists, and reflect the potential community scale solar water heating to reduce energy consumption and emissions without additional assumptions about changes to urban form.

3.1.2 Technical Limitations

Unlike community scale PV systems, the physical nature of solar thermal systems limits the size of the geographies they can serve. Transmission losses from hot water distribution networks may be as large as 30%, even if pipes are buried and insulated according to code.¹⁰⁷ The performance of the community scale solar water heating systems considered in this study are more sensitive to total transmission distance than are systems with heat injection loops.

Transmission Losses

The efficiency and cost-effectiveness of central heating systems generally increase with scale, but the superior performance of large systems is due in part to how such systems store and transmit thermal energy. In district scale heating systems, heat injection loops act as thermal storage tanks, reducing the need for heated fluid to travel long distances through comparatively narrow pipes to reach users, thus minimizing transmission losses.¹⁰⁸

Future residential construction projects may include heat storage loops, but the expense and complexity of retrofitting existing residential housing stock with central heat injection loops makes such an approach infeasible. Instead, transmission losses may be diminished by selecting residential parcels that are both densely constructed and populated.

3.2 System and Property Ownership

¹⁰³ Masunaga, S. (9 April 2009). *Co-gen helps UCLA go green*. The Daily Bruin. Retrieved from: <http://dailybruin.com/2009/04/09/co-gen-helps-ucla-go-green/>

¹⁰⁴ ConEdison. (2018). *Steam Service*. Retrieved from: <https://www.coned.com/en/commercial-industrial/steam>

¹⁰⁵ San Francisco Department of the Environment. (2018). *District Heating*. Retrieved from: <https://sfenvironment.org/article/geothermal/district-energy>

¹⁰⁶ District Energy St. Paul. (2018). *District Heating*. Retrieved from: <http://www.districtenergy.com/technologies/district-heating/>

¹⁰⁷ Anderson, K.R. (12 March 2018). Personal Communication.

¹⁰⁸ Chen, W. (21 February 2018). Personal Communication.

Community scale SWH systems installed in LA County cannot take advantage of existing thermal energy infrastructure; thus, SWH system owners must bear the costs of construction and operation, offset by the applicable incentives. Land ownership patterns, utility billing practices, laws, and policies regarding SHW system financing all limit the number of candidate sites for community scale SWH that are available within LA County.

3.2.1 Land Use Patterns

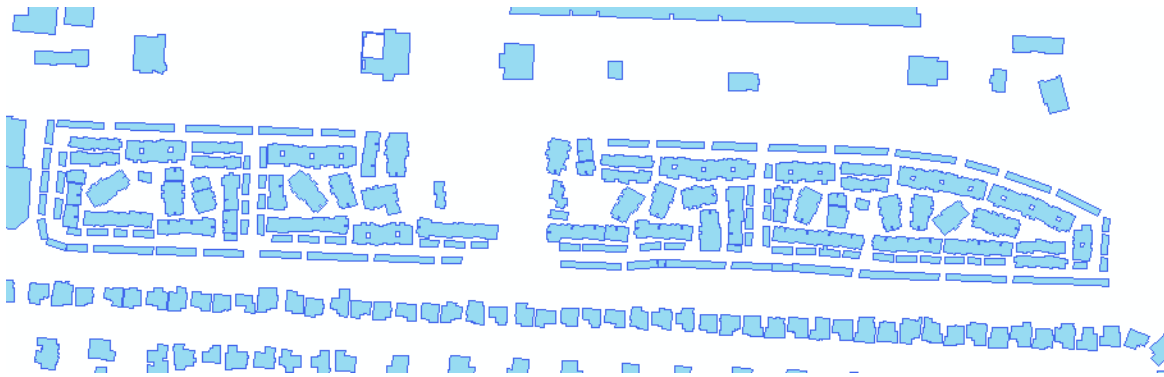
LA County's diversity of urban forms and patchwork of single and multi-family residential buildings increases the complexity of designing and building a SWH system that serves multiple properties and residences. Land use and ownership patterns affect the size of the geographies community scale energy systems may serve, and foremost among the factors constraining the size of community scale SWH systems is the separation of residential parcels by roadways.

Los Angeles is among the densest cities in the U.S., and correspondingly, has a relatively high roadway mileage per capita.¹⁰⁹ The extension of community scale systems beyond single parcels or city blocks would require system owners to secure permission from local authorities to lay insulated pipe across roadways. In the interest in minimizing uncertainty about system costs, the community scale SWH systems considered in this study will serve either single or contiguous groups of parcels. In some cases, energy communities may be spread over multiple parcels separated by streets, but in such an instance separate parcels will be served by separate community-scale SWH systems.

Figure 10: Aerial Image (Above) and Building Outlines (Below) for the Pheasant Ridge Apartments in Rowland Heights, CA.



¹⁰⁹ Manville, M., & Shoup, D. (2004). Parking, People, and Cities. <https://doi.org/10.1061/ASCE0733-94882005131:4233>

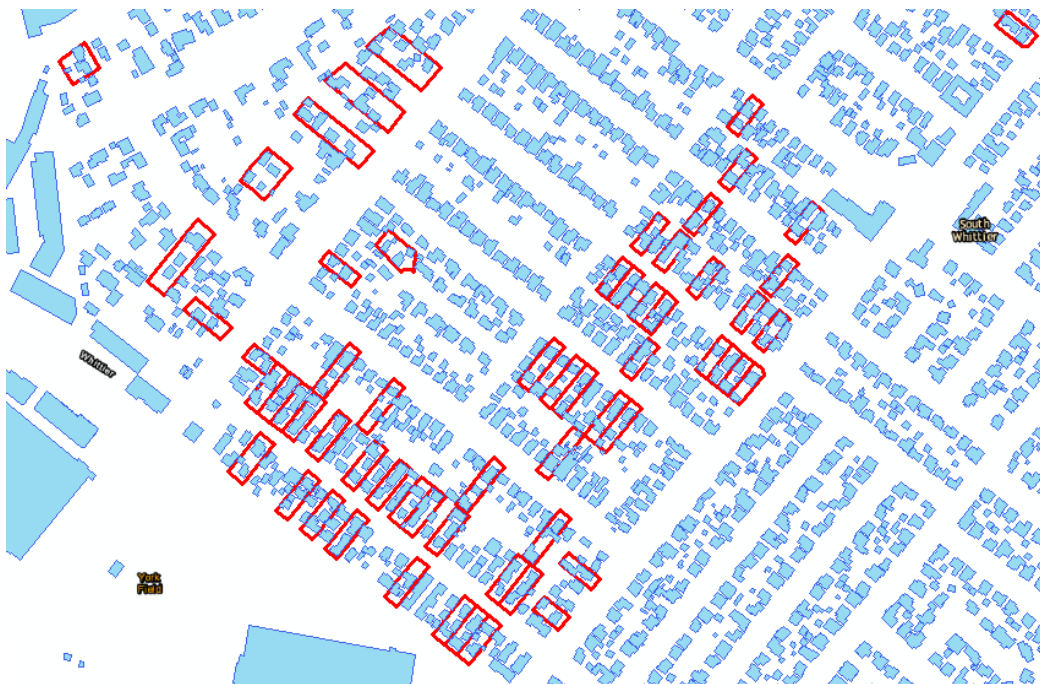


Source: LARIAC5 Orthogonal Imagery & Building Outlines Dataset

3.2.2 Collective Ownership

Theoretically, community scale solar water heating systems could be constructed and operated like thermal microgrids: with a mixture of distributed and centralized collection and storage, depending on the population density and urban form of a given site. Such a system would need to be owned collectively by the people it serves, who pay for the cost of its construction and maintenance, one which could perhaps be offset in part by government incentives. While it may be possible to construct and operate such a community scale SWH system, collective ownership of a community scale system is presently infeasible.

Figure 11. Adjacent Properties with 1 AIN (Single Owner) in Whittier, California



The image above (building outlines from aerial LiDAR) shows groups of adjacent residential properties (in red) where collective ownership of a solar water heating system is possible.

Source: LARIAC5 Orthogonal Imagery & Building Outlines Dataset

Communities intending to construct a collectively owned thermal microgrid like the one described in the previous paragraph face considerable transaction costs, and must structure and manage relationships between users and the firms who design, build, and manage the energy infrastructure.¹¹⁰ This is a significant departure from how thermal energy is currently generated and distributed for residential use, and is the primary reason collectively owned systems are not considered in this study.

Secondly, collectively owned community scale SWH systems are also ineligible for state and federal incentives.¹¹¹ This study considers only community scale SWH systems that are eligible for California's CSI-Thermal Multifamily Rebate, and the Federal Residential Renewable Energy Tax Credit. Specific technological and property qualifications for each are discussed in the *Solar Water Heating Report*.

The state thermal rebate and renewable tax credits are designed to offset the capital cost of solar water heating systems for the sole owner of a structure (or, more generally, a residential property) upon which the systems are installed. This is the third reason why collective ownership arrangements are considered to be outside the scope of this study. In order for a residential parcels to be considered a candidate energy community for solar water heating, those parcels must have single owner to which incentive payments can be made.

3.3 Candidate Case Study Site Pools

This section explains how a programmatic and explicable case study selection method is developed from the broader constraints on community scale SWH in LA County. The first subsection describes how absolutely qualifying/disqualifying characteristics are used to select large pools of candidate energy communities from the Energy Atlas's parcel data.¹¹² The second discusses the development and application of a parcel scoring metric for community scale SWH suitability. Parcel rankings and other practical considerations are then used to select case study sites.

3.3.1 Development of Public & Private Residential Parcel Pools

Selection of case study sites begins with the Energy Atlas's two million tax assessor's parcels.¹¹³ In order to select the public and private residential parcels on which community scale SWH is

¹¹⁰ Gui, E. M., Diesendorf, M., & MacGill, I. (2017). Distributed energy infrastructure paradigm: Community microgrids in a new institutional economics context. *Renewable and Sustainable Energy Reviews*, 72, 1355-1365. <https://doi.org/10.1016/J.RSER.2016.10.047>

¹¹¹ Chen, W. (7 June 2018). Personal Communication.

¹¹² California Center for Sustainable Communities. (2018). *Los Angeles County Megaparcel*s [Data set].

¹¹³ Ibid.

feasible, the search filter described in Table 2 is applied.¹¹⁴ The table below summarizes the set of parcel characteristics that make community scale SWH broadly feasible.

Table 11: Public and Private Property Energy Community Filter Criteria

Desired Energy Community Characteristics	Filter Conditions
Energy communities may have more than one building per site	Building Count ≥ 1
Energy communities must have more than one residential unit per site	Residential Units > 1
	First two digits of LA County Tax Assessor’s Parcel Database Usecode indicate multi-family dwelling (02XX-05XX)
Minimize the number of parties involved in construction and operation	<ul style="list-style-type: none"> - For Private Parcels: 1 AIN associated with a private residential parcel. - For Public Parcels: Public parcels must have structures and facilities owned and operated by LA City or County
Parcels must have a single owner or ownership entity to which incentive payments can be made.	

The results of the query are as follows:

Table 12: Public & Private Parcel Counts from Community Scale SWH Filter

Private Parcels	Public Parcels
~19, 000 Multi-Family/ Mixed-Use Parcels	213 City and County Public Housing Parcels

As mentioned previously, the community scale filter identifies residential parcels where community scale solar water heating is feasible, but does not include any notion of how well-suited a particular parcel is to a community scale approach to solar water heating. To select specific case study site programmatically requires ranking different residential parcels according to their suitability for a community scale SWH system. This study’s ranking is based on the available parcel data and the geographic and building-level variables known to influence

¹¹⁴ Ibid.

the performance of SWH systems.^{115,116,117} The ranking and selection method for private and public parcels is described below.

3.3.2 Parcel Suitability Ranking and Selection Method

Community scale SWH case study sites will be chosen according to the following criteria:

1. **Parcel SWH Suitability Score**
2. **Number of Residential Units per Parcel**
3. **Urban Form and Climatic Considerations**

A residential parcel's suitability score is given by the following expression:

Equation 5. Parcel Suitability Score

$$\text{Parcel Suitability Score} = \frac{\left(\frac{U_N A_B}{B_N P_B}\right)}{A_P}$$

Where:

- U_N = Number of residential units per parcel
- A_B = Sum of building footprint areas on a parcel
- B_N = Number of buildings per parcel (with building outline $\geq 300 \text{ ft}^2$)
- P_B = Sum of building footprint perimeters on a parcel
- A_P = Area of the parcel

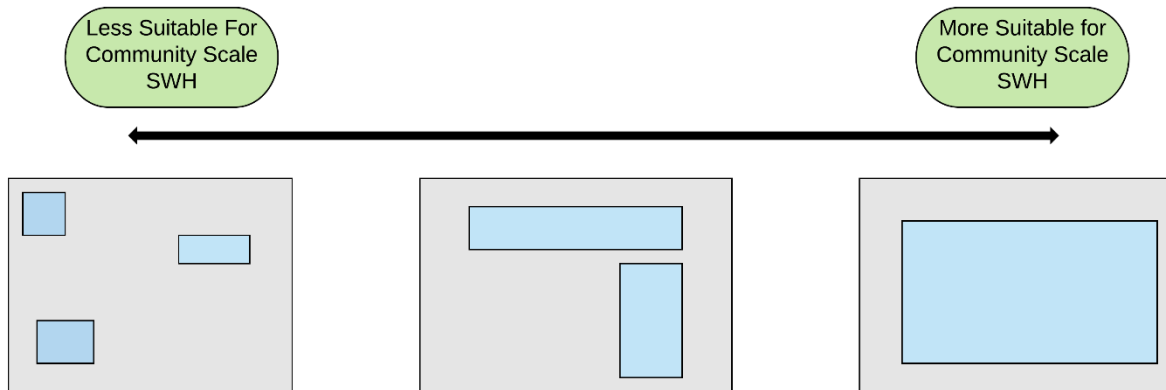
Parcels with higher ratios of building area to parcel area, and parcels with greater population densities (residential units/ unit parcel area) score better than parcels with more numerous buildings, lower built area ratios, and fewer residential units. The relationship is illustrated in Figure 12:

¹¹⁵ Dongellini, M., Falcioni, S., & Morini, G. L. (2015). Dynamic simulation of solar thermal collectors for domestic hot water production. *Energy Procedia*, 82, 630–636. <https://doi.org/10.1016/j.egypro.2015.12.012>

¹¹⁶ ASPE. (2015). Domestic Hot Water Systems, (March).

¹¹⁷ Marini, D., Buswell, R., & Hopfe, C. J. (2015). A critical software review - how is hot water modelled in current building simulation. Retrieved from <https://dspace.lboro.ac.uk/2134/19285>

Figure 12. Parcel Suitability Score



The suitability score encapsulates how a parcel’s built environment influences the performance and capital cost of a hydronic solar water heating system or systems. Parcels with small, distantly spaced structures may have insufficient rooftop space for collector arrays, possibly necessitating installation of collector arrays on the ground. Furthermore, long runs of insulated hot water pipe between storage tanks and residential units will increase both the cost of the system (both for materials and trenching), as well as heat loss. By contrast, parcels with fewer, larger, and more densely populated structures may adopt SWH at a lower cost, and without installing additional heat transmission infrastructure.

Because the suitability score computes a ratio of areas weighted by residential units and the number of buildings, it will also necessary to consider the absolute number of residential units. Case studies with different numbers of residential units (between 10-1000 units) will be chosen to elucidate the effect of population density on SWH system performance and design.

3.4 Residential Parcel Ranking and Selection – Public & Private Cases

3.4.1 Private Parcel Ranking and Selection Method

There are approximately 19,000 privately owned parcels in LA County for which community scale SWH is feasible. From this pool, three instructive cases were selected using the following data:

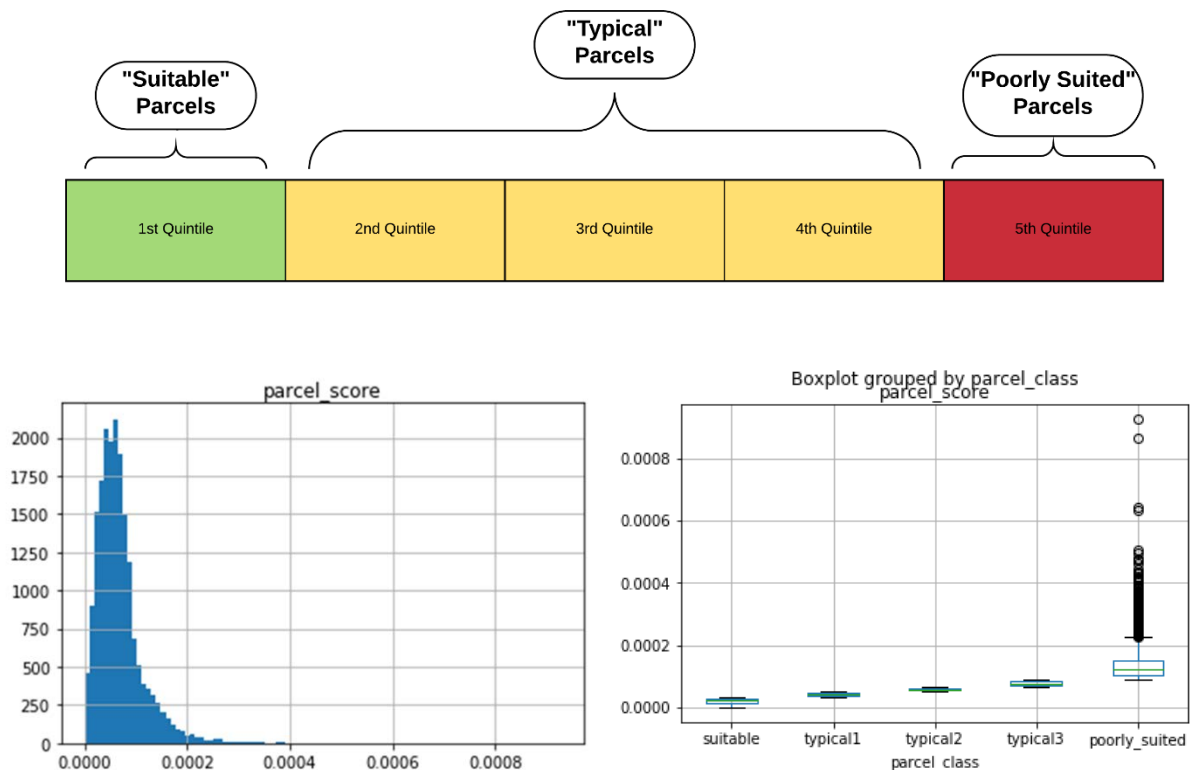
Table 13. Private Parcel Data

Variable	Description	Data Source
Building Count	Number of buildings per residential parcel with roof area > 300 ft ² .	LARIAC 4 Building Outlines
Unit Count	Number of residential units per residential parcel.	Energy Atlas

Parcel Area	Parcel area in m ² .	Energy Atlas
Parcel Perimeter	Parcel perimeter in m.	Energy Atlas
Building Area	Area of the <i>i</i> th building's outline on the <i>j</i> th residential parcel in m ² .	LARIAC 4 Building Outlines
Building Perimeter	Perimeter of the <i>i</i> th building's outline on the <i>j</i> th residential parcel in m.	LARIAC 4 Building Outlines

The first step in selection of private cases was to compute the parcel suitability score for each of the parcels in the private pool. The parcels are then divided into quintiles (~3000 parcels each) and classified according to their scores. Figure 13 illustrates the suitability ranking scheme, and shows the distribution of scores among the parcels:

Figure 13. Parcel Ranking Scheme and Distribution of Parcel Suitability Scores by Quintiles



After sorting each quintile by counts of residential units per parcel, a “suitable” case was selected from the first quintile, a “typical” case from the middle three quintiles, and a “poorly-suited” case from the 5th quintile. These cases were selected based on their parcel score, the number of residential units in each energy community, and the presence of other potentially

instructive variation in urban form. Finally, if a parcel selected is part of a larger community (i.e. one parcel of an apartment complex spanning multiple parcels), the entire community is selected.

3.4.2 Public Parcel Ranking and Selection

Selection of publically owned residential parcels began with the aggregation of the City and County Housing Authorities' asset portfolios. The Housing Authority of the City of Los Angeles (HACLA) and the Housing Authority of the County of Los Angeles (HACoLA) publish the addresses of the properties that they own and maintain. These properties meet the sole ownership requirement discussed in Table 11, but further information was needed from the Energy Atlas database and other sources to develop a list of feasible properties.

Table 14. Public Property Parcel Data

Variable	Description	Data Source
Asset Location	HACLA/HACoLA Asset Portfolio addresses geocoded to tax assessor's parcel locations	HACLA Asset Portfolio, HACoLA Asset Portfolio, Google Geocoding API, Energy Atlas
Building Count	Number of buildings per residential parcel with roof area > 300 ft ² .	LARIAC 4 Building Outlines
Unit Count	Number of residential units per residential parcel.	Energy Atlas, City of Los Angeles Health Atlas ¹¹⁸
Parcel Area	Parcel area in m ² .	Energy Atlas
Parcel Perimeter	Parcel perimeter in m.	Energy Atlas
Building Area	Area of the <i>i</i> th building's outline on the <i>j</i> th residential parcel in m ² .	LARIAC 4 Building Outlines
Building Perimeter	Perimeter of the <i>i</i> th building's outline on the <i>j</i> th residential parcel in m.	LARIAC 4 Building Outlines

First, the lists of addresses for properties owned by both housing authorities were geocoded to associate them with their corresponding assessor's parcels. This step is essential for scoring

¹¹⁸ County of Los Angeles Public Health. (2013). *LA Subsidized Housing Units (2008) from the Health Atlas for the City of Los Angeles July 2013* [GIS Dataset]. Retrieved from: <http://www.arcgis.com/home/item.html?id=419689b020704eae90221f086eb9815c>

and selection as the number of buildings and residential units is required. Google's Geocoding API was used to accomplish this task.¹¹⁹

Two-hundred and thirteen HACLA and HACoLA residential parcels met the feasibility requirements listed in Section 2.1. The selection of case studies from the pool of 213 candidate parcels follows a similar procedure (scoring and sorting by number of residential units per parcel) to the private parcels. If a parcel belonging to a larger public housing site or development is selected, then the entire site is selected as a case study. Considering the smaller size of the public parcel pool, the following cases are chosen to represent the diversity in public housing stock.

¹¹⁹ Google Maps Platform. (2018). *Developer Guide – What is Geocoding?*
<https://developers.google.com/maps/documentation/geocoding/intro>.

Chapter 4: Community Scale Solar Water Heating Case Studies

4.1 Community Scale SWH System Sizing and Site-Specific Hot Water Demand Calculations

The tasks of estimating the energy savings from a specific solar water heating system, and evaluating the emissions reduction potential of community scale solar water heating in general, are complicated by the lack of a standard approach to SWH system design, and the difficulty inherent in estimating domestic hot water demand from a limited set of generally publicly available building-level variables. Also, most extant community scale solar heating systems provide energy for both space and water heating, and are sometimes embedded within larger district-scale heating systems. SWH system performance data that can be made is scarce.^{120, 121} Thus, in order to evaluate the performance of community scale systems appropriate for Los Angeles County's climate and built environment, a simulation based approach must suffice.

The following sections describe the simplifying assumptions, programmatic specification and sizing of the 102 SWH systems simulated for this study. Simulation parameters are based on building characteristics and the occupancy limits of the residential units within them. The calculation of domestic hot water demand based on technical assumptions published by the American Society of Heating, Refrigerating and Air-Conditioning Engineers (ASHRAE) is also addressed.^{122, 123} The following sections detail the programmatic specification of the three most influential simulation parameters: collector area, storage volume, and domestic hot water demand. Other simulation parameters and their values are listed in Appendix 2.

4.1.1 Community Scale SWH System Design and Components.

As described in the Chapter 1, community scale solar water heating systems in Los Angeles County are hydronic, active, and closed. Regardless of scale, the SWH systems simulated in this study consist of physically separate thermal collection and potable hot water distribution loops. The collection loop is filled with a glycol-water mixture to protect against freezing and stagnation, and heat is transferred to potable water in a system's solar storage tank through an immersed heat exchanger. The systems simulated in this study are consistent with the

¹²⁰ Fisch, M. N., Guigas, M., & Dalenbäck, J. O. (1998). A review of large-scale solar heating systems in Europe. *Solar energy*, 63(6), 355-366.

¹²¹ Pinel, P., Cruickshank, C. A., Beausoleil-Morrison, I., & Wills, A. (2011). A review of available methods for seasonal storage of solar thermal energy in residential applications. *Renewable and Sustainable Energy Reviews*, 15(7), 3341-3359.

¹²² American Society of Plumbing Engineers. (2015). *Domestic Hot Water Systems: Continuing Education from The American Society of Plumbing Engineers*. Retrieved from: https://www.aspe.org/sites/default/files/webfm/ContinuingEd/CEU_221_Mar15.pdf

¹²³ Goldner, F. S., & Price, D. C. (n.d.). Domestic Hot Water Loads, System Sizing and Selection for Multifamily Buildings. Retrieved from https://acee.org/files/proceedings/1994/data/papers/SS94_Panel2_Paper12.pdf

requirements listed in California’s Title 24 and the CSI-Thermal Handbook.¹²⁴ ¹²⁵ All systems for community scale SWH consist of the following elements:

Table 15. Community Scale Solar Water Heating System Components

Component	Description
Solar Thermal Collector Panels	- Model: SunEarth EP-40 4x10 Collector Panels
Storage Tank	- 100 – 2000+ gallons - Immersed load-side heat exchanger - R12 insulation
Insulated Copper Pipe	- 1' copper pipe for collector and distribution loops.
Control Unit	- Control and monitor flow and temperature in t
Expansion Tank	- System stagnation protection
Auxiliary Heater	- Gas water heater/ central boiler - Distributed or centralized depending on site
Circulation Pumps	- 40 – 100 W pumps for collector and distribution loops

4.1.2 Parcel-Scale vs. Structure-Scale Community Solar Water Heating

Prior to running SWH system simulations and interrogating the results, it is first necessary to determine whether it is feasible or desirable to build community scale SWH systems that serve an entire residential parcels rather than separate residential structures. Studies of extant systems suggest that larger, centralized systems exhibit superior thermal efficiency than similarly designed smaller one, and in some instances deliver heat at a lower cost.¹²⁶ ¹²⁷

However, in the context of Los Angeles County, the price of natural gas, building code and rebate requirements, and the material costs of construction negate any potential benefits from the installation of a parcel-level system.

While modest economies of scale are observed for residential solar water heating systems (approximately \$120/ ft² collector area for large systems vs. \$160/ ft² collector area for single family homes), these cost savings reflect the fact that larger, more monolithically structured systems require fewer control units, pumps, and other equipment per square foot of collector

¹²⁴ California Solar Initiative. (2016). *California Solar Initiative Handbook-Thermal*. (2018). Retrieved from http://www.gosolarcalifornia.ca.gov/documents/CSI-Thermal_Handbook.pdf

¹²⁵ California Energy Commission. (2015). *2016 Residential Compliance Manual*. Retrieved from: <http://www.energy.ca.gov/2015publications/CEC-400-2015-032/CEC-400-2015-032-CMF.pdf>

¹²⁶ Chen, W. (18 June 2018). Personal Communication.

¹²⁷ US Army Corps of Engineers. (2011). *Central Solar Water Systems Design Guide*. Retrieved from: https://www.wbdg.org/FFC/ARMYCOE/COEDG/dg_solar_hot_water.pdf

area.¹²⁸ Residential retrofits also typically make use of the installed gas or electric water heaters as the system's auxiliary heater to reduce capital cost.¹²⁹

The low price of natural gas necessitates that even in ideal retrofit cases (i.e. a building with a central water heater and adequate roof area, for which data on actual demand exists) residential SWH systems must, at minimum, qualify for the CSI-Thermal performance based incentive to be economically viable.¹³⁰ To date, systems that serve multiple residential structures do not qualify for the CSI-Thermal Performance Based Incentive or the federal Residential Renewable Energy Tax Credit.¹³¹ ¹³² Parcel-scale SWH systems intended to serve multiple residential structures may also require additional labor, materials, and equipment. Depending on the application, centralized, parcel-scale SWH systems serving multiple structures may require buried and insulated pipe, additional auxiliary heating equipment (such as gas-condensing boilers) and specialized control units.¹³³

The relationship between the scale and performance of hydronic solar thermal systems of the type described previously, and the technical challenges posed by the construction of large, centralized SWH systems are not well understood, and thus, considered to be outside the scope of this study. However, efforts to reduce emissions from the residential housing sector would benefit from a better understanding of the aforementioned topics.

4.1.3 Collector Area and Storage Volume Parameters

With component technologies for community scale SWH selected, and the question of parcel-scale vs. structure-scale scale settled, the next task is to programmatically size each SWH system according to the building characteristics that are publicly available. As mentioned previously, there is no one canonical method for sizing SWH systems and predicting system performance; a variety of computational approaches can be considered as valid.¹³⁴ ¹³⁵ System sizing is also an iterative process. In most instances rough sizing guidelines are used as a starting point for a series of system simulations until a performance target or targets are achieved.¹³⁶

¹²⁸ Bavin, T. (15 June 2018). Personal Communication.

¹²⁹ Chrisman, A. (4 May 2018). Personal Communication.

¹³⁰ Chen, W. (5 July 2018). Personal Communication

¹³¹ California Solar Initiative. (2016). California Solar Initiative Handbook-Thermal. (2018). Retrieved from http://www.gosolarcalifornia.ca.gov/documents/CSI-Thermal_Handbook.pdf

¹³² US Department of Energy. (2018). *Residential Renewable Energy Tax Credit*. Retrieved from: <https://www.energy.gov/savings/residential-renewable-energy-tax-credit>

¹³³ Bavin, T. (5 July 2018). Personal Communication.

¹³⁴ Duffie, J. A., & Beckman, W. A. (2013). Solar engineering of thermal processes. John Wiley & Sons.

¹³⁵ Anderson, K.R. (10 June 2018). Personal Communication.

¹³⁶ ¹³⁶ Bavin, T. (5 July 2018). Personal Communication

This study relies on two widely used system sizing ratios to determine an initial collector area and storage volume. The collector area/ storage volume ratio used in this study is also a requirement of CA Title 24.¹³⁷

Table 16. Sizing Ratios for Collector Area & Solar Tank Storage Volume

Collector Area / Storage Volume	Storage Volume / Conditioned Area
$\frac{1 \text{ sqft collector area}}{1.5 - 2.0 \text{ gallons storage tank volume}}$	$\frac{90 \text{ gallons storage tank volume}}{2000 \text{ sqft conditioned area}}$

Thus, solar tank volume and collector area for a given SWH system are functions of the structure’s *conditioned area*, or floor space.

For various reasons, exact square footage figures were not available for any of the buildings included in this study. Housing authorities and development site staff could not locate the appropriate records in most cases. In lieu of exact square footages, conditioned area was determined using the building outline and height measurements included in the LARIAC Building Outlines shapefile.¹³⁸The LARIAC Building Outlines shapefile contains building heights, areas, and elevations for all the structures with area > 300 ft² in LA County. Building dimensions are estimated from aerial LiDAR data acquired by EagleView Inc. using a proprietary algorithm. The conditioned area for a building is given by the following equation:

Equation 6. Conditioned Area Formula

$$C_A = \frac{B_H}{10} * B_A$$

Where:

C_A = Conditioned Area

B_H = Building Height

B_A = Building Outline Area

The formula above provides an estimate of floor square footage assuming 10 ft. of building height per floor. The results of this calculation were checked, and in some cases modified using LARIAC’s most recent oblique aerial imagery.¹³⁹ Manual measurements were taken from orthogonal aerial imagery for buildings consisting of multiple wings with different numbers of floors.

¹³⁷ California Solar Initiative. (2016). California Solar Initiative Handbook-Thermal. (2018). Retrieved from http://www.gosolarcalifornia.ca.gov/documents/CSI-Thermal_Handbook.pdf

¹³⁸ Los Angeles Regional Imagery Acquisition Consortium. (2017). 2017 LA County Building Outlines [dataset]. EagleView, Inc.

¹³⁹ Los Angeles Regional Imagery Acquisition Consortium. (2017). LARIAC 5 LA County Oblique Imagery. EagleView, Inc.

4.1.4 Residential Hot Water Demand Schedule and Calculations

It is difficult to produce accurate estimates of domestic hot water consumption based a small set of building and occupant characteristics.¹⁴⁰ Actual consumption of hot water has been found to vary within $\pm 30\%$ of estimates calculated from technical assumptions.¹⁴¹ Thus, for the purposes of this study, calculated hot water demand and the implied gas and water consumption per residential unit for each case study site must meet the following criteria prior to being used for simulations:

1. **Calculated water and gas consumption values must fall within the distribution of actual water and gas consumption per unit from the Energy Atlas database.**
2. **The volume of hot water consumed per month must be < 8 HCF per unit.**

The volume of water consumed per month must be less than the maximum consumption for Tier 1 LADWP residential consumers (800 cubic feet per residential account per month).¹⁴² To check the robustness of the hot water demand assumptions, a comparison is made between the hot water consumption calculated from technical assumptions and actual consumption values from the CCSC Energy Atlas database.

This study uses standard technical assumptions published by ASHRAE and American Society of Plumbing Engineers (ASPE) to calculate daily hot water demand on a per person basis.^{143, 144} Hot water demand on the basis of a person-day for a residential building is calculated from the following:

- **Hot Water Event Types** – Depending on what appliances and hot water fixtures present in a residential unit, such a dishwashers or washer/dryers, the set of hot water “events” are the possible end-uses of hot water.
- **Hot Water Volume per Event** – ASHRAE and ASPE list average volumes of hot water at draw-off temperature (120°F) consumed per event type (see Table 17). These volumes are different the total volume of water (hot and cold) used per event. Total hot water consumption is assumed to be 1/3 to 1/2 of the total indoor water consumption.
- **Event Frequency per Person-Day/ Person-Month** – The frequency of hot water events are determined on daily and monthly bases. Daily events are assumed to occur once or more per day, and monthly events once or more per month. Event frequencies vary between cases, and are listed in each case study.
- **Maximum Occupancy per Residential Unit** – Maximum allowable occupancy per unit is determined by housing authority rules, or stipulated by the owners of private residential buildings.

¹⁴⁰ Fuentes, E., Arce, L., & Salom, J. (2018). A review of domestic hot water consumption profiles for application in systems and buildings energy performance analysis. *Renewable and Sustainable Energy Reviews*, 81(February 2017), 1530-1547. <https://doi.org/10.1016/j.rser.2017.05.229>

¹⁴¹ *Ibid.*

¹⁴² Los Angeles Department of Water & Power. (2016). *2016-2020 Water & Power Rate Changes - About Our New Water Tiers*. Retrieved from: https://d3n8a8pro7vhmx.cloudfront.net/ladwp/pages/41/attachments/original/1464888325/2016Rates_Tiers-v2.pdf?1464888325

¹⁴³ Kalogirou, S. A. (2013). *Solar energy engineering: processes and systems*. Academic Press.

¹⁴⁴ ASPE. (2015). *Domestic Hot Water Systems Handbook*.

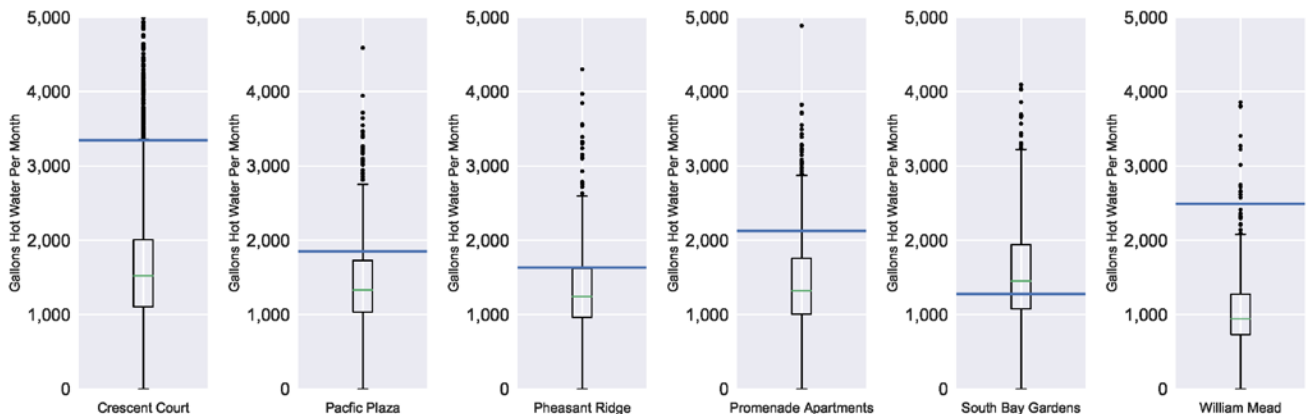
Table 17. Hot Water Volume per Event Type¹⁴⁵

Event Type	Daily/Monthly Basis	Volume HW Consumed (gal)
Food Preparation	Daily	3.96
Manual Dishwashing	Daily	3.96
Shower	Daily	3.96
Bath	Monthly	15.85
Face & Hand Washing	Daily	2.64
Dishwasher (per wash cycle)	Monthly	6.00
Clothes Washing (per wash cycle)	Monthly	36.00

The CCSC’s Energy Atlas’s historical water and gas consumption data for LA County provides the actual per unit gas and water consumption values to which calculated values are compared. To check if calculated consumption values meet the criteria above, water and gas consumption data for samples of properties similar to each case study were drawn from the database.

Samples of actual water and gas consumption values were selected using binned sampling to ensure an adequate number of observations and representativeness. Samples were selected based on binned vintage (year of construction), parcel square footage, and the number of residential units. Figures 18 and 19 show calculated per unit consumption values (blue horizontal lines) and distributions of actual per unit consumption values (box plots) for each case study.

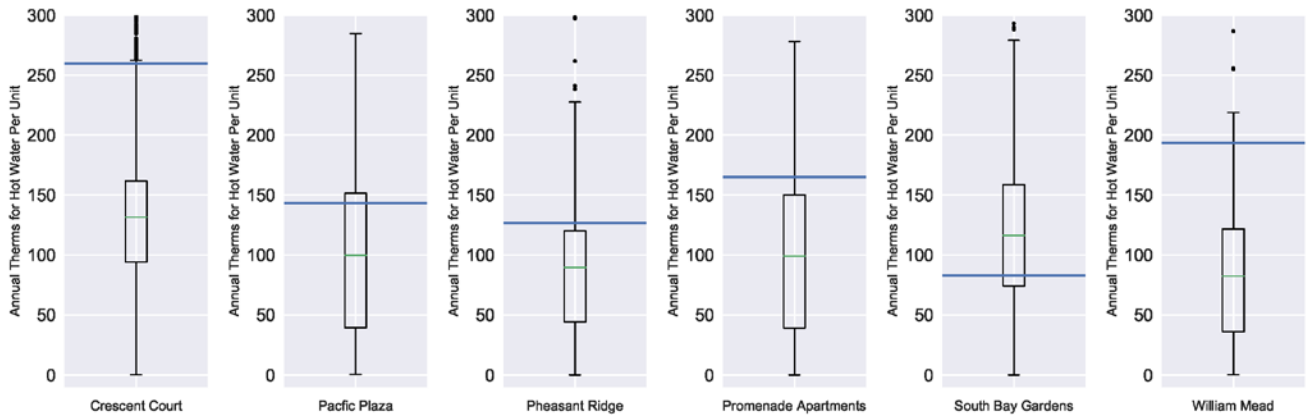
Figure 18: Calculated and Actual Monthly Water Consumption per Residential Unit for Case Study Sites and Comparison Samples



Source: CCSC Energy Atlas Database

¹⁴⁵ Ibid.

Figure 19: Calculated and Actual Annual Gas Consumption per Residential Unit for Case Study Sites and Comparison Samples



Source: CCSC Energy Atlas Database

Actual gas and water consumption meet the criteria stipulated above, however, comparison is complicated by the fact that actual consumption values are influenced by occupancy levels.

4.2 Community Scale Solar Water Heating Case Studies – Private Cases

4.2.1 Suitable Case – Pheasant Ridge Apartments, Rowland Heights, CA.

The Pheasant Ridge Apartments is a large residential complex with approximately 600 1-and 2-bedroom units on two residential parcels, divided by an entrance road. Pheasant Ridge is composed of seventy residential structures, as well as covered parking and utility and management buildings. Rowland Heights is located in the far south eastern portion of Los Angeles County.

Figure 20. Location of the Pheasant Ridge Apartments

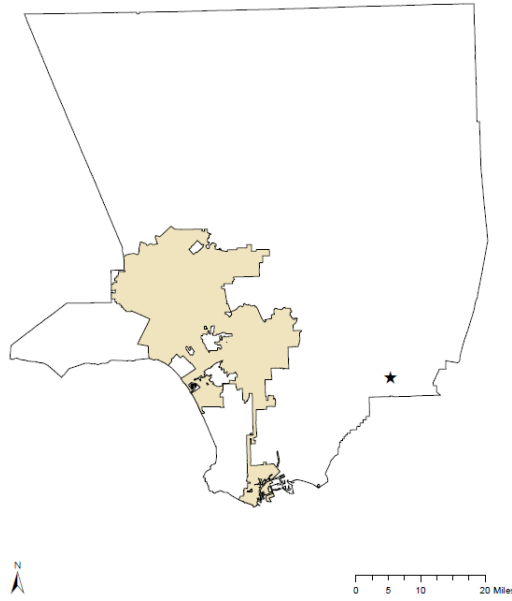
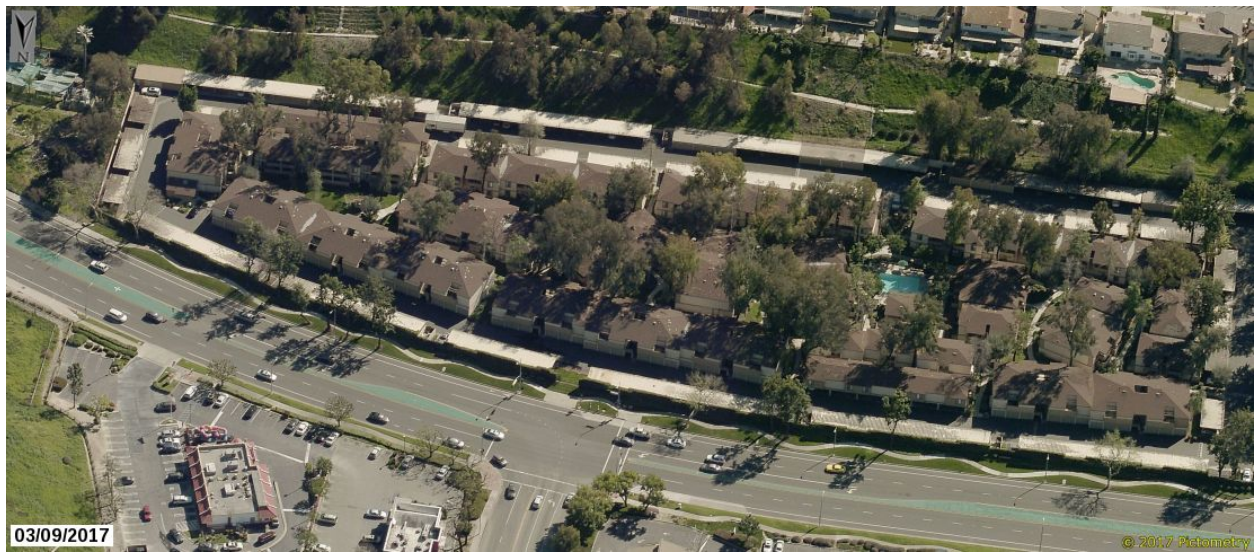
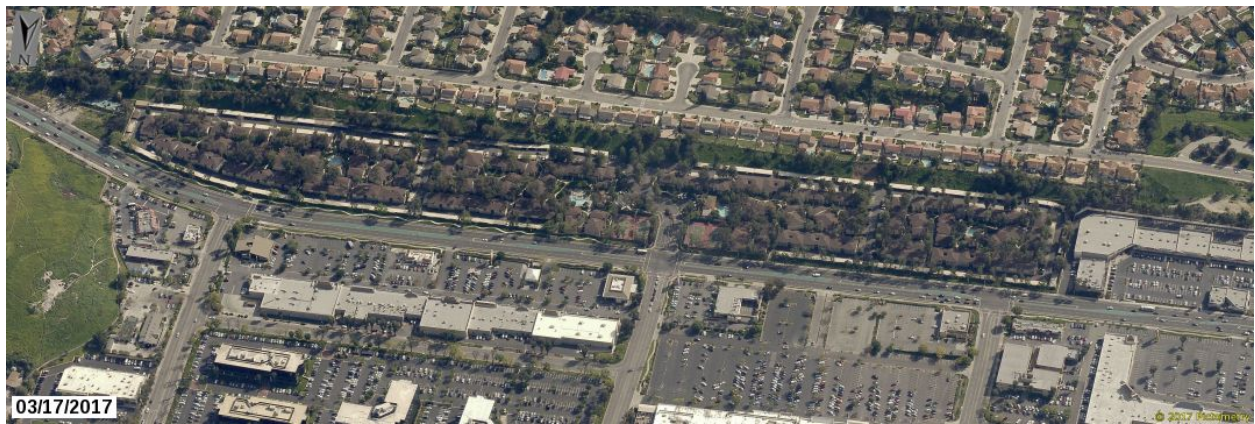


Figure 21. Aerial Images of Pheasant Ridge Apartment Complex



Oblique aerial photographs of the Pheasant Ridge Apartment complex. The site occupies 4 large residential parcels near a major shopping center in the City of Rowland Heights

Source: LARIAC/ EagleView Inc.

Pheasant Ridge is well-suited to community scale solar water heating due to its size and density. However, the pitched roofs of the buildings, and the presence of large trees on the property complicate installation of collector arrays, and possibly reduce the performance of systems installed on the site.

Based upon publically available information and conversations with complex’s management company, the following information will be used to parameterize hot water demand schedules and SWH system simulations:

Table 18. Pheasant Ridge Site Data

Site Area	99286.9 m ²
Site Perimeter	1939.54 m
Residential Units	620
Residential Structures	71
Current Water Heating Technology	Units have individual gas heaters
Additional Information	2-bedroom units contain dishwashers, 3 shared laundry facilities.

Pheasant Ridge Apartments - Hot Water Demand and Conditioned Area Calculations

Pheasant Ridge site managers cooperated with requests for a site visit and provided a site map, unit floorplans illustrations, and an estimate of the number of 1-bedroom units with dishwashers (approximately 60% of 1-bedroom units have dishwashers).¹⁴⁶ Based on this information, the maximum occupancies of units, the set of possible hot water events, and event frequencies were determined:

Table 19. Pheasant Ridge - Hot Water Events & Event Frequencies

¹⁴⁶

Event	Total Flow (120°F Draw-off)	Basis & Per Person Frequency
Food Preparation	3.96	2x Daily
Manual Dish Washing	3.96	2x Daily
Shower	3.96	1x Daily
Bath	15.85	1x Monthly
Face and Hand Washing	2.64	2x Daily
Dish Washer	6.00	12x Monthly
Clothes Washing	36.00	3x Monthly

Pheasant Ridge offers 1 and 2 bedroom units for rent. Maximum occupancy for 1-bedroom units is assumed to be 2 persons. 2-bedroom units are assumed to have a maximum occupancy of 4 persons. No manual dishwashing was assumed to occur in units with dishwashers. The conditioned areas for each of Pheasant Ridge’s structures is determined according to Equation 6. The Pheasant Ridge hot water demand schedule implies the following monthly water and annual gas consumption per residential unit.

Table 20. Pheasant Ridge - Calculated Water and Gas Consumption Values

Annual Gas Consumption per Residential Unit	3710.86 kWh/ 126.65 therm
Monthly Water Consumption per Residential Unit	18740.2 gal/ 2.46 HCF

The water and gas consumption values calculated from the Pheasant Ridge hot water demand schedule are near the third quartiles of the distributions of actual gas and water consumption (see Figures 18 and 19), and meet the consumption criteria described in Section 4.1.4. No further adjustment of the hot water demand schedule was necessary prior to system simulations. Distributions actual and water and gas consumption values for comparison come from properties with the following characteristics:

Table 21. Comparison Property Sample Characteristics

Property Characteristics	Database Query Criteria
Construction Vintage	1990 or Later
Parcel Square Footage	>50,000 ft ²

Number of Res. Units	>100 Units
Parcel Usetype	Multifamily

Pheasant Ridge Apartments - System Design & Simulation Results

Building-level system simulations for Pheasant Ridge (with the system design and hot water demand described above) yield the following results:

Table 22. Site Summary of Pheasant Ridge’s SWH Simulation Results

Performance Metrics	Values
Average Annual System Energy	25184.598310 kWh
Average Solar Fraction	0.750559 (75.1% solar energy for water heating)
Average Annual Heat Delivered	30853.782715 kWh
Average Annual Auxiliary Heat Required w/ Solar	8193.384321 kWh
Average Annual Heat Delivered - Auxiliary Only	3.348961e+04 kWh

Pheasant Ridge’s SAM simulation results show that, with the baseline system specifications for residential SWH systems, Pheasant Ridge can displace approximately 75% of the gas consumed for water heating. This level for performance qualifies the site for both the Residential Renewable Energy Tax Credit and the CSI-Thermal Performance Based Incentive.

Figure 22. Pheasant Ridge – Average Monthly SWH System Energy & Average Auxiliary Energy per Month.

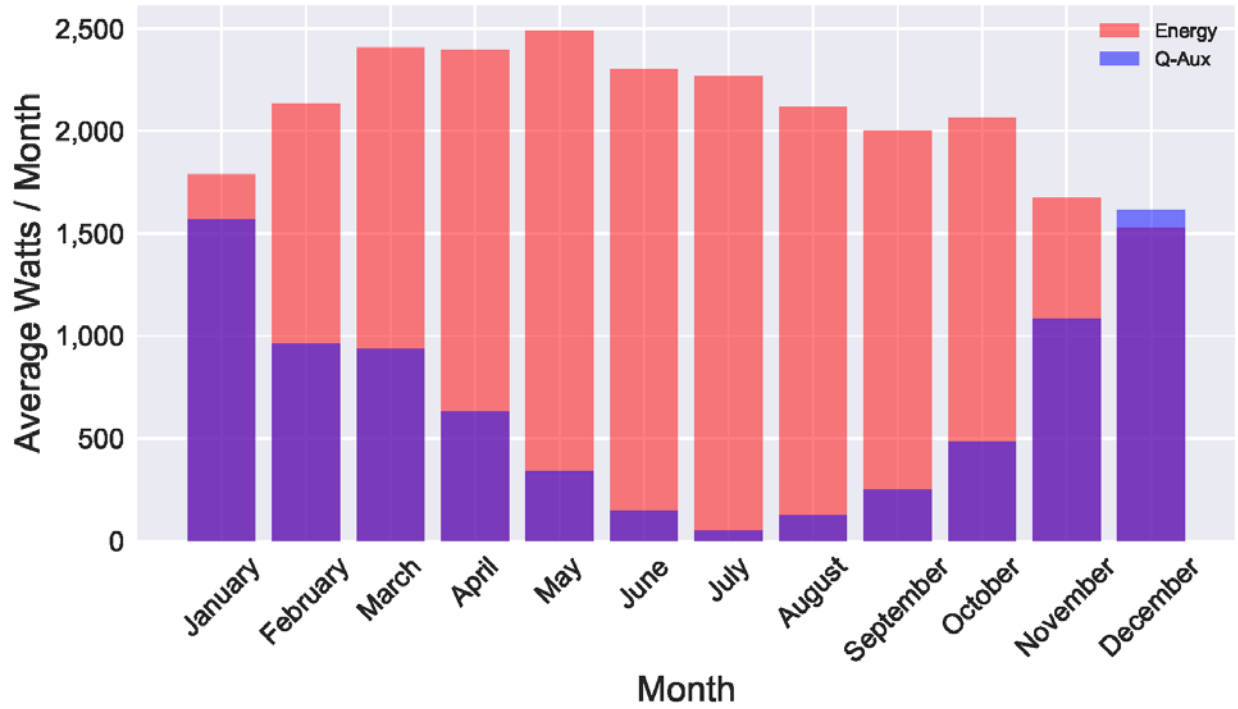
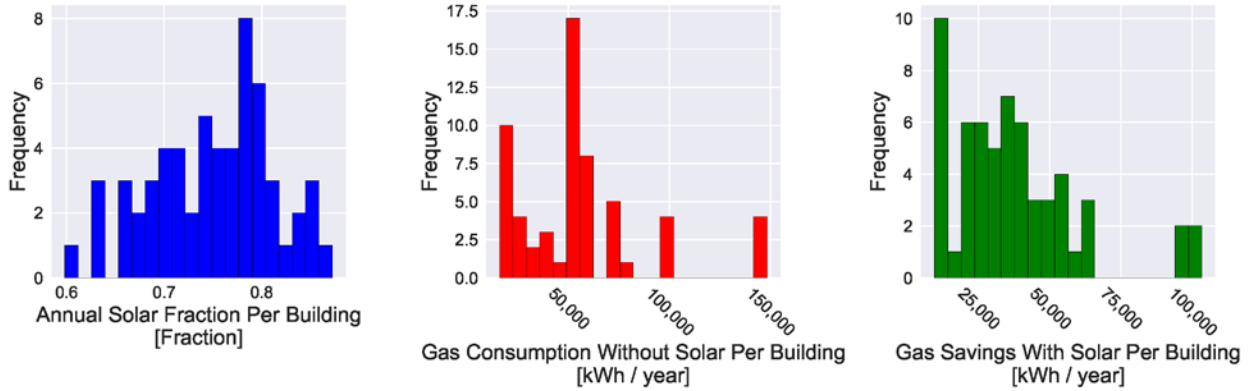


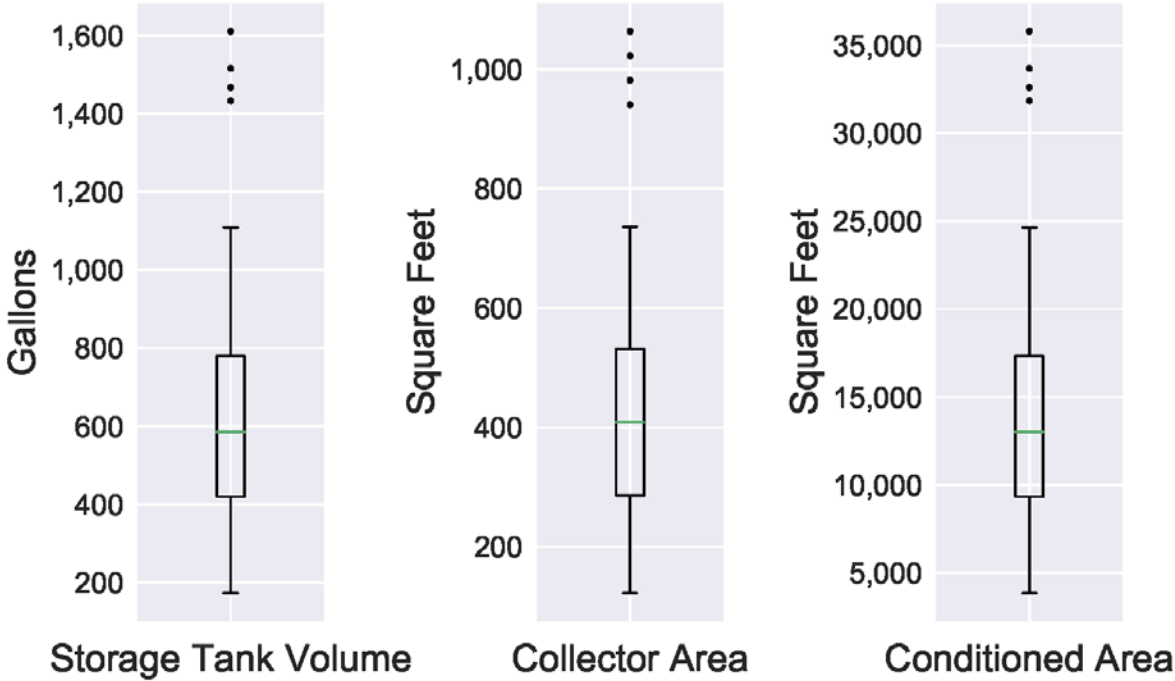
Figure 22 shows the average watts per month generated by the SWH systems installed in each building. As expected, SHW systems perform best in the summer months, with site solar fraction reaching a maximum in July. The only month for auxiliary heaters provide more energy than SWH systems is December.

Figure 23. Pheasant Ridge – Solar Fraction, Gas Consumption w/o SWH, and Gas Savings per Building.



The histograms in Figure 23 show the distribution of solar fraction, gas consumption, and gas savings across the ~70 residential structures on the 4 residential parcels that make up Pheasant Ridge. Individual solar fractions for SWH systems range from approximately 53% to >90%. All of the SWH systems meet the minimum performance requirement set by Title 24 (>20% average annual solar fraction).

Figure 24. Pheasant Ridge – Collector Areas, Tank Volumes, and Conditioned Areas for SWH System Simulations.



The baseline assumptions for conditioned area and system sizing for Pheasant Ridge produce the distributions of tank volume and collector area shown in Figure 8. Storage tanks range from 100-2000 gallons, and collector area from 100-1500 ft². The range of collector areas roughly corresponds to 2-25 individual collector panels.

4.2.2 Typical Case – Promenade Apartments, West Covina, CA.

The Promenade Apartments is a 124-unit affordable housing complex located near the I-10 Freeway in the San Gabriel Valley, East of downtown Los Angeles. The complex offers studio and 1-bedroom apartments, rented preferentially to families and seniors at below-market rates.¹⁴⁷ National CORE, a non-profit housing and community outreach organization, owns and manages the property.

Figure 25. Location of the Promenade Apartments

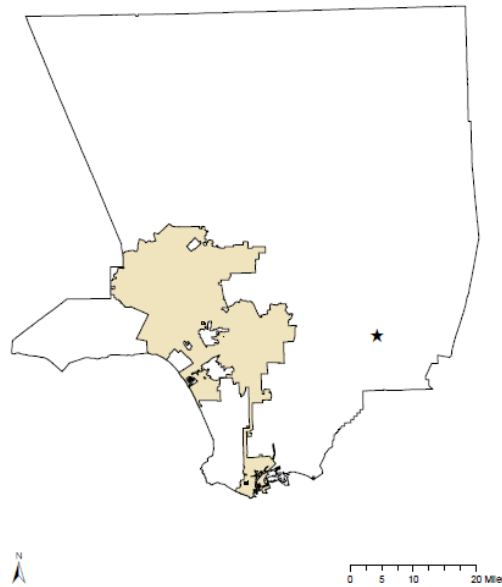


Figure 26. Aerial Images of the Promenade Apartments, West Covina, CA.



¹⁴⁷ National Community Renaissance. (2018). *About Us*. Retrieved from: <http://nationalcore.org/about-us/>



The Promenade Apartments are a private-nonprofit affordable housing complex located due north of the 60 Freeway in West Covina.

Source: LARIAC/ EagleView, Inc.

The Promenade Apartments represent typical medium-density apartment complexes common in LA County. The property features centralized laundry facilities, but residential units contain their own storage water heating units.

Promenade Apartments is owned and managed by National Community Renaissance, a nonprofit organization that offers subsidized housing and other supportive and educational services to families.¹⁴⁸

Table 23. The Promenade Apartments Site Data

Site Area	9032.49 m ²
Site Perimeter	309.64 m
Residential Units	124
Residential Structures	1
Current Water Heating Technology	1 storage water heater per unit
Additional Information	1-bedroom units contain dishwashers, shared laundry facilities.

¹⁴⁸ National CORE. (2018). *About Us*. Retrieved from: <https://nationalcore.org/about-us/>

Pheasant Ridge Apartments - Hot Water Demand and Conditioned Area Calculations

Despite repeated attempts to contact both the Promenade Apartments site staff and National CORE, no representative from the residential complex or the nonprofit that manages operations and programs at other properties responded to requests for information. The site’s hot water demand schedule was determined using the number of each unit type and the floorplans listed on the property’s publicly available website. The floorplans indicated the presence or absence of dishwashers and washer/dryer units.¹⁴⁹

Table 24. Promenade Apartments - Hot Water Events & Event Frequencies

Event	Total Flow (120°F Draw-off)	Basis & Per Person Frequency
Food Preparation	3.96	2x Daily
Manual Dish Washing	3.96	2x Daily
Shower	3.96	1x Daily
Bath	15.85	1x Monthly
Face and Hand Washing	2.64	2x Daily
Dish Washer	6.00	12x Monthly
Clothes Washing	36.00	3x Monthly

Promenade Apartments offers studio and 1-bedroom units for rent. Maximum occupancy for a studio units is assumed to be 2 persons. One-bedroom units are assumed to have a maximum occupancy of 4 persons. It was assumed that no manual dishwashing was assumed to occur in units with dishwashers. The conditioned area of the Promenade Apartments complex is determined according to Equation 6.

The Promenade Apartments’ hot water demand schedule implies the following monthly water and annual gas consumption per residential unit:

Table 25. Promenade Apartments - Calculated Water and Gas Consumption Values

Annual Gas Consumption per Residential Unit	4839.79 kWh/ 165.18 therm
Monthly Water Consumption per Residential Unit	2126.14 gal/ 2.84 HCF

¹⁴⁹ National Community Renaissance. (2017). *Promenade Apartments*. Retrieved from: <https://nationalcore.org/property-details/promenade/>

The water and gas consumption values calculated from the Promenade Apartments hot water demand schedule are just above the third quartiles of the distributions of actual gas and water consumption (see Figures 18 and 19), and meet the consumption criteria described in Section 1.2.1. No further adjustment of the hot water demand schedule was necessary prior to system simulations. Distributions of actual water and gas consumption values for comparison come from properties with the following characteristics:

Table 26. Promenade Apartments - Comparison Property Sample Characteristics

Property Characteristics	Database Query Criteria
Construction Vintage	1950 - 1978
Parcel Square Footage	10,000 – 20,000 ft ²
Number of Res. Units	>100 Units
Parcel Usetype	Multifamily

Promenade Apartments - System Design & Simulation Results

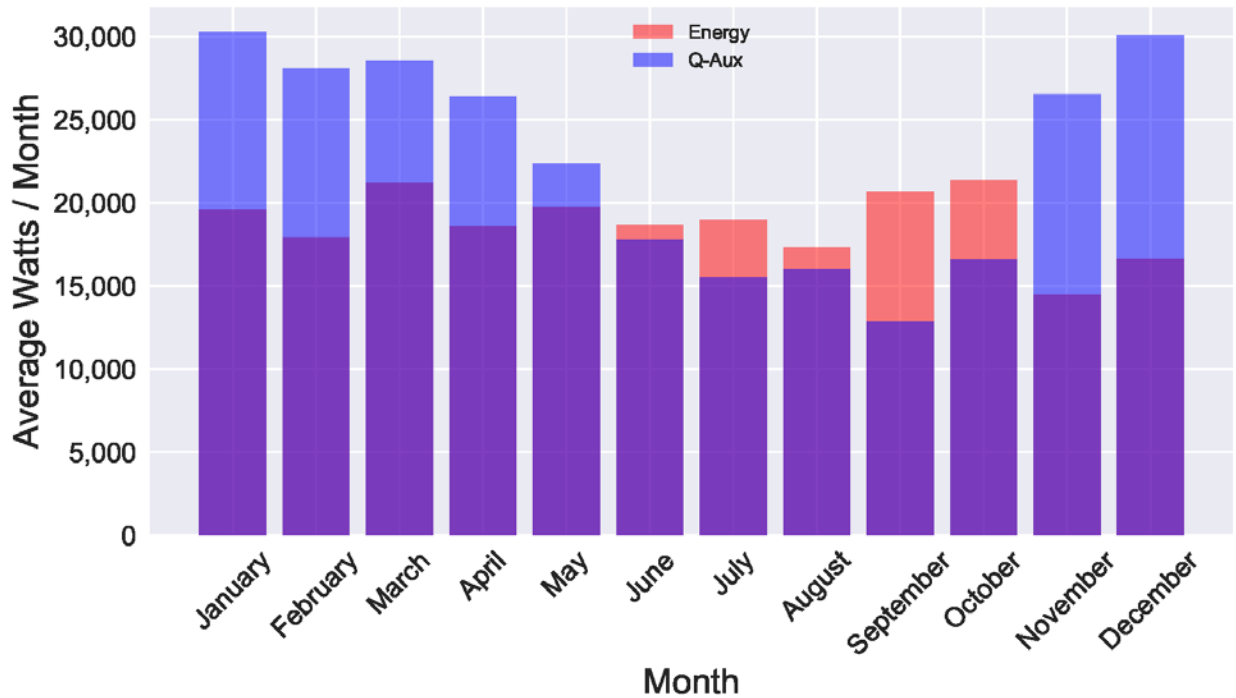
Building-level system simulations for the Promenade Apartments (with the system design and hot water demand described above) yield the following results:

Table 27. Promenade Apartments – Site Summary of SWH Simulation Results

Performance Metrics	Values
Average Annual System Energy	224984.95 kWh
Average Solar Fraction	0.453434 (45.3% solar energy for water heating)
Average Annual Heat Delivered	343389.031 kWh
Average Annual Auxiliary Heat Required w/ Solar	270963.156 kWh
Average Annual Heat Delivered - Auxiliary Only	4.961807e+05 kWh

Using the baseline system sizing assumptions, the Promenade Apartment’s SWH system meets Title 24 requirements and qualifies for the CSI-Thermal performance based incentive. The site’s system also displaces approximately half of the gas consumed for water heating.

Figure 27. Promenade Apartments – Average Monthly SWH System Energy & Average Monthly Auxiliary Energy



Unlike Pheasant Ridge, the Promenade Apartment’s system energy is relatively constant between months, and considerable quantities of auxiliary energy are required to meet demand between November and May.

Table 27. Promenade Apartments –Gas Consumption w/o SWH, and Gas Savings per Building.

Annual Gas Consumption w/o SWH System	826967 kWh/ year
Gas Savings w/ SWH System	418767 kWh/ year

Table 27 shows the annual consumption of gas implied by the hot water demand schedule with and without the site’s SWH system. Table 28 shows the collector area, the number of collector panels, tank volume, and conditioned area for the site.

Table 28. Promenade Apartments – Collector Area, Tank Volume, and Conditioned Area for SWH System Simulation.

Collector Area	2985.91 ft ²
Collector Panels	73
Solar Tank Volume	4509.03 gals

Conditioned Area	100201 ft ²
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4.2.3 Poorly Suited Case – Pacific Plaza, Santa Monica, CA.

The Pacific Plaza is a mixed-use high-rise apartment building with approximately 500 studio and 1-bedroom units.

Figure 29. Location of the Pacific Plaza

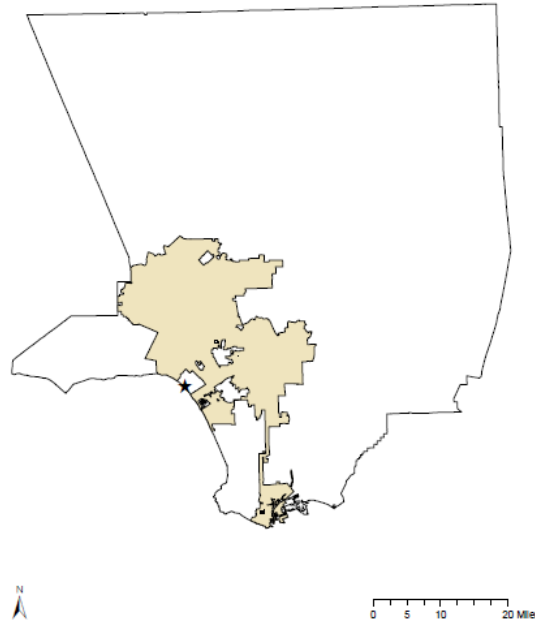


Figure 30. Aerial Images of the Pacific Plaza Building





Pacific Plaza offers very little rooftop space relative to the other sites, and is the densest development in terms of residential units per parcel area included in this study. Furthermore, it may be necessary to locate solar storage tanks in the basement of the building if there is insufficient space for them on the rooftop.

Table 28. Pacific Plaza Site Data

Site Area	2330.16 m ²
Site Perimeter	194.45 m
Residential Units	288
Residential Structures	1
Current Water Heating Technology	1 storage water heater per unit
Additional Information	1-bedroom units contain dishwashers, shared laundry facilities.

Pacific Plaza - Hot Water Demand and Conditioned Area Calculations

Pacific Plaza is owned and maintained by Douglas Emmett, a publically-traded real estate investment firm with a portfolio of residential and commercial properties.¹⁵⁰

¹⁵⁰ Douglas Emmett. (2018). *Corporate Profile*. Retrieved from: <https://www.douglasemmett.com/our-story>

Table 29. Pacific Plaza - Hot Water Events & Event Frequencies

Event	Total Flow (120°F Draw-off)	Basis & Per Person Frequency
Food Preparation	3.96	2x Daily
Manual Dish Washing	3.96	2x Daily
Shower	3.96	1x Daily
Bath	15.85	1x Monthly
Face and Hand Washing	2.64	2x Daily
Dish Washer	6.00	12x Monthly
Clothes Washing	36.00	3x Monthly

Pacific Plaza offers studio and 1-bedroom units with various configurations for rent at market rates. Maximum occupancy for a studio units is assumed to be 2 persons, and 1-bedroom units are assumed to have a maximum occupancy of 3 persons. No manual dishwashing is assumed to occur in units with dishwashers. The conditioned area of the building is determined according to Equation 6.

Pacific Plaza’s hot water demand schedule implies the following monthly water and annual gas consumption per residential unit:

Table 30. Pacific Plaza - Calculated Water and Gas Consumption Values

Annual Gas Consumption per Residential Unit	4205.58 kWh/ 143.53 therm
Monthly Water Consumption per Residential Unit	1847.69 gal/ 2.47 HCF

The calculated water and gas consumption values implied by Pacific Plaza’s hot water demand schedule meet the consumption criteria described in Section 4.2.1. Monthly water consumption per residential unit is slightly greater than the third quartile of the comparison distribution, and annual gas consumption per unit is at the upper end of the inter-quartile range. No further adjustment of the hot water demand schedule was necessary prior to system simulations. Distributions actual and water and gas consumption values for comparison come from properties with the following characteristics:

Table 31. Pacific Plaza - Comparison Property Sample Characteristics

Property Characteristics	Database Query Criteria
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Construction Vintage	1950 - 1978
Parcel Square Footage	>50,000 ft ²
Number of Res. Units	>100 Units
Parcel Usetype	Multifamily

Pacific Plaza - System Design & Simulation Results

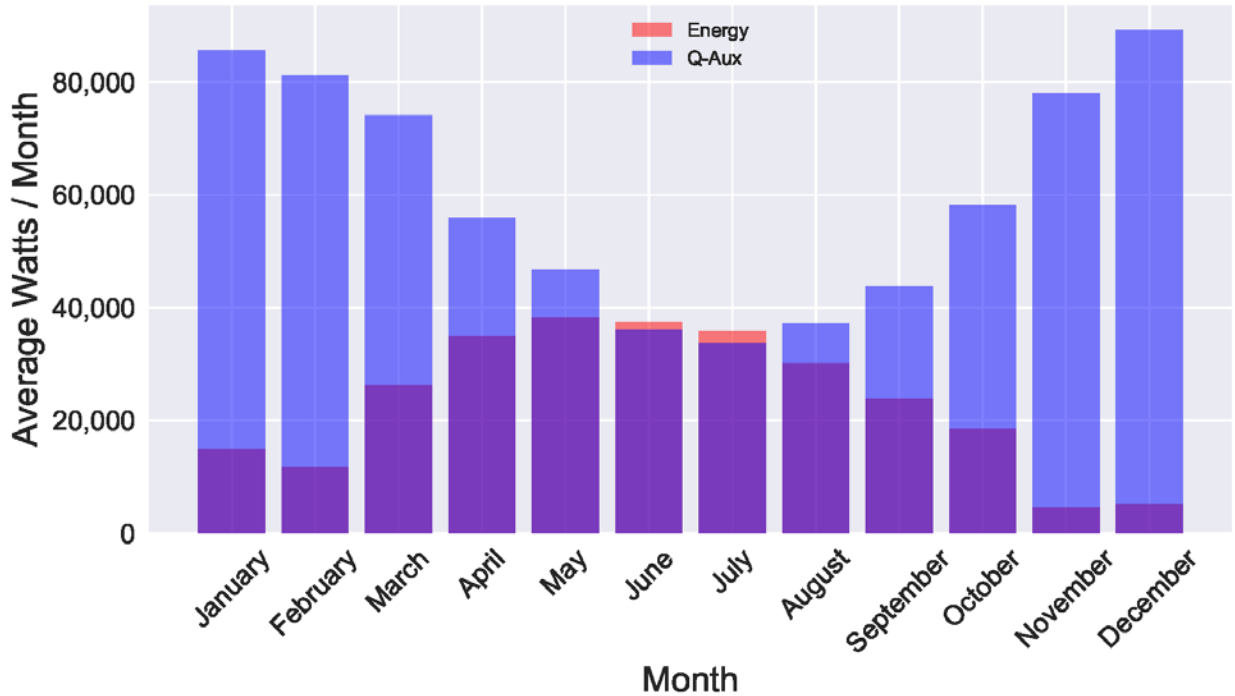
The baseline demand and sizing assumptions produce the following results for Pacific Plaza's SWH system:

Table 32. Pacific Plaza – Site Summary of SWH Simulation Results

Performance Metrics	Values
Average Annual System Energy	281267.53 kWh
Average Solar Fraction	0.2809 (28.1% solar energy for water heating)
Average Annual Heat Delivered	723295.69 kWh
Average Annual Auxiliary Heat Required w/ Solar	719816.63kWh
Average Annual Heat Delivered - Auxiliary Only	1.001394e+06 kWh

Pacific Plaza's SWH system meets the minimum requirements of Title 24, and qualifies for the CSI-Thermal performance-based incentive. However, Pacific Plaza's relatively low annual solar fraction (<50%) means that the SWH system does not qualify for the federal Residential Renewable Rebate.

Figure 31. Pacific Plaza – Average Monthly SWH System Energy & Average Monthly Auxiliary Energy



The only months for which Pacific Plaza’s hot water demand is met with more solar energy than gas are during those with the greatest number of daylight hours. Pacific Plaza’s proximity to the ocean may also explain the low system energy relative to the other case studies. Early morning and evening clouds diminish incident radiation, and limiting the performance of the building’s SWH system.

Table 33. Pacific Plaza –Gas Consumption w/o SWH, and Gas Savings with SWH.

Annual Gas Consumption w/o SWH System	1,668,989 kWh/ year
Gas Savings w/ SWH System	882,068 kWh/ year

Table 33 shows the annual consumption of gas implied by the hot water demand schedule with and without the site’s SWH system. Table 34 shows the collector area, the number of collector panels, tank volume, and conditioned area for the site.

Table 34. Pacific Plaza – Collector Area, Tank Volume, and Conditioned Area for SWH System Simulation.

Collector Area	9039.53 ft ²
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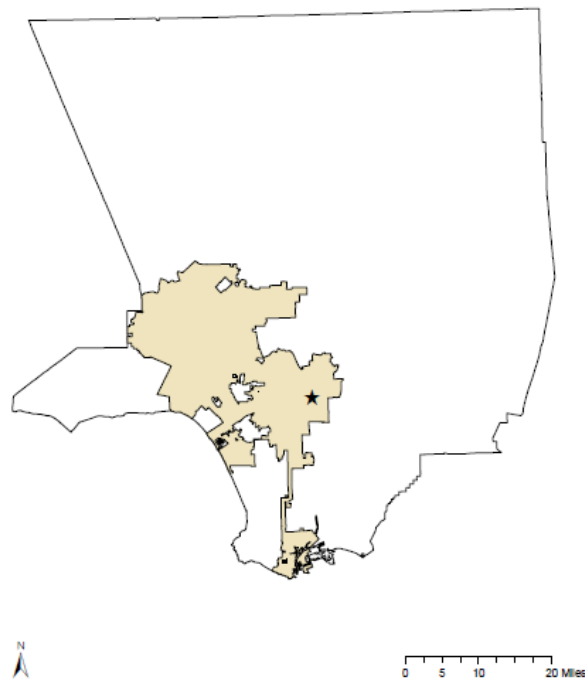
Collector Panels	221
Solar Tank Volume	13532.81 gals
Conditioned Area	300730 ft ² (rooftop area: 16164.80 ft ²)

4.3 Community Scale Solar Water Heating Case Studies – Public Cases

4.3.1 Suitable Case – William Mead Homes, Los Angeles, CA.

The William Mead Homes are a public housing development located in the Lincoln Heights neighborhood of Los Angeles. The site consists of 24, 2- and 3-story residential buildings and 415 units. HACLA manages and maintains the property, which was built by the federal government in 1945.¹⁵¹ Families with children are given preference for open units.

Figure 32. Location of the William Mead Homes



¹⁵¹ HACLA. (2017). *About Public Housing*. Retrieved from: <http://home.hacla.org/aboutpublichousing>

Figure 33. Aerial Images of the William Mead Homes



The William Mead Homes are high-density residential buildings with flat, unobstructed roof areas. The style of construction is ideal for the placement of rooftop collector arrays. There is also ample room near the buildings to construct small sheds that would be needed to house SWH system storage tanks.

Table 35. William Mead Homes Site Data

Site Area	83656.84 m ²
Site Perimeter	1425.1 m
Residential Units	415
Residential Structures	24
Current Water Heating Technology	30-gal A.O. Smith Gas Storage WH/ Unit
Additional Information	No dishwashers. ~50% of units have washing machines

William Mead Homes - Hot Water Demand and Conditioned Area Calculations

A site map, descriptions of the unit floorplans, and information about installed water heaters were obtained during a visit to the William Mead Homes. Maintenance staff and site managers cooperated with all requests for information.¹⁵² The Housing Authority of the City of Los Angeles also provides maximum occupancy limits based on a unit’s number of bedrooms.¹⁵³ Based on this information, the maximum occupancies of units, the set of possible hot water events, and event frequencies were determined:

Table 36. William Mead Hot Water Events & Event Frequencies

Event	Total Flow (120°F Draw-off)	Basis & Per Person Frequency
Food Preparation	3.96	2x Daily
Manual Dish Washing	3.96	1x Daily
Shower	3.96	1x Daily
Bath	15.85	1x Monthly
Face and Hand Washing	2.64	2x Daily
Clothes Washing	36.00	2x Monthly

The William Mead Homes public housing complex offers units ranging in occupancy from 2 to 8 people based on the number of bedrooms in each unit. Greater than half the number of units

¹⁵² Santa Ana, A.F. (10 April 2018). Personal Communication.

¹⁵³ Housing Authority of the City of Los Angeles. (2017). *How to Apply for Public Housing*. Retrieved from: <http://home.hacla.org/applyforph>

have a maximum of 4. Each unit contains a washer-dryer hookup, but a washer-dryer unit is not an included amenity. The maintenance staff estimated that approximately 50% of the units have washer-dryers installed.¹⁵⁴ Washer-dryer units were assigned randomly to 50% of the units for demand calculations. None of the units have dishwashers, only manual dishwashing is assumed to occur.

The conditioned areas for each of William Mead’s 24 structures were calculated with building outline measurements made in EagleView’s CONNECTExplore aerial imagery web application, and Equation 6.¹⁵⁵ About half of the site’s buildings’ wings have different numbers of floors. Manual measurement of the building wings’ rooftop areas were used to calculate conditioned area for each wing. The conditioned areas of each wing were then added to find the conditioned area of a given building.

William Mead’s hot water demand schedule implies the following monthly water and annual gas consumption per residential unit.

Table 37. William Mead Calculated Water and Gas Consumption Values

Annual Gas Consumption per Residential Unit	3710.86 kWh/ 126.65 therm
Monthly Water Consumption per Residential Unit	2603.22 gal/ 3.48 HCF

The water and gas consumption values calculated from the William Mead hot water demand schedule are at the upper ends of their respective distributions, but meet the consumption criteria described in Section 4.2.1. William Mead’s water and gas consumption per unit reflects the fact that most public housing developments are fully occupied, and that larger units are frequently taken by families with children.¹⁵⁶ Distributions actual and water and gas consumption values for comparison come from properties with the following characteristics:

Table 37. Comparison Property Sample Characteristics

Property Characteristics	Database Query Criteria
Construction Vintage	Pre-1950
Parcel Square Footage	>50,000 ft ²
Number of Res. Units	>100 Units

¹⁵⁴ Santa Ana, A.F. (10 April 2018). Personal Communication.

¹⁵⁵ EagleView, Inc. (2018). *CONNECTExplorer - Web-based imagery access and analysis*. Retrieved from: <https://www.eagleview.com/product/imagery-viewing-platforms/connectexplorer/>

¹⁵⁶ Santa Ana, A.F. (10 April 2018). Personal Communication.

Parcel Usetype	Multifamily
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William Mead - System Design & Simulation Results

The William Mead Homes complex consists of 24 residential buildings. Each building has its own SWH system serving the units contained within. Table 20 shows the system performance metrics averages across the site’s 24 buildings:

Table 38. William Mead – Site Summary & SWH Simulation Results

Performance Metrics	Values
Average Annual System Energy	42400.77 kWh
Average Solar Fraction	0.460812 (46.1% solar energy for water heating)
Average Annual Heat Delivered	49219.69 kWh
Average Annual Auxiliary Heat Required w/ Solar	49395.817790 kWh
Average Annual Heat Delivered - Auxiliary Only	9.193374e+04 kWh

Pheasant Ridge’s SAM simulation results show that, with the baseline system specifications for residential SWH systems, Pheasant Ridge can displace approximately 75% of the gas consumed for water heating. This level for performance qualifies the site for both the Residential Renewable Energy Tax Credit and the CSI-Thermal Performance Based Incentive.

Figure 34. William Mead – Average Monthly SWH System Energy & Average Monthly Auxiliary Energy.

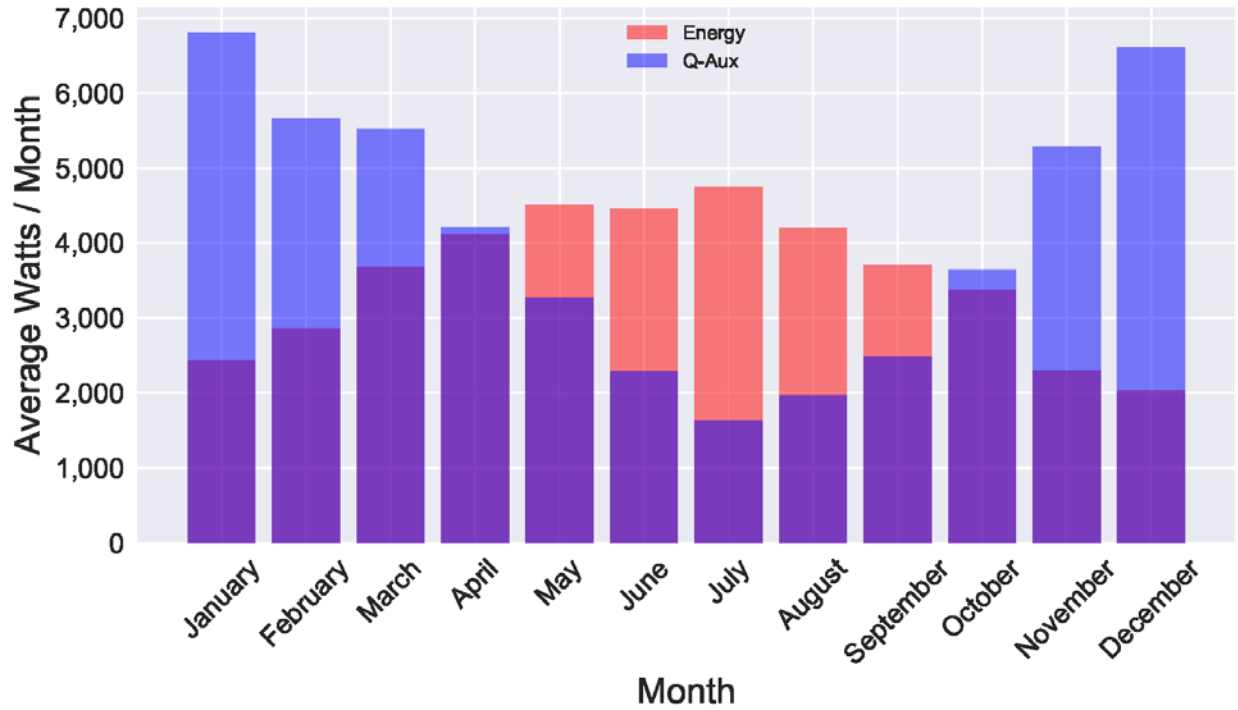
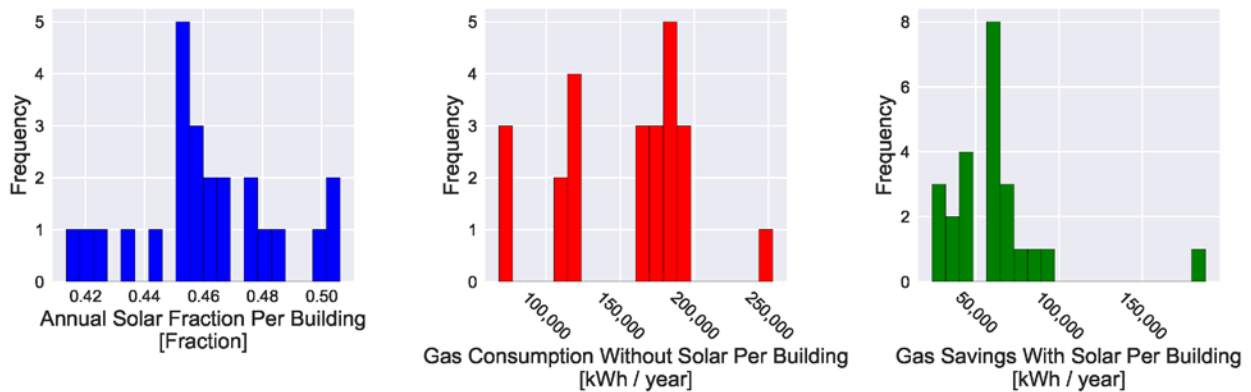


Figure 34 shows the watts per month of solar energy captured and auxiliary generated by the SWH system for the average William Mead building. The average William Mead SWH system performs best during the 5 summer months, meeting hot water demand with more solar energy than auxiliary gas. From October to April, auxiliary gas energy is required to meet hot water demand.

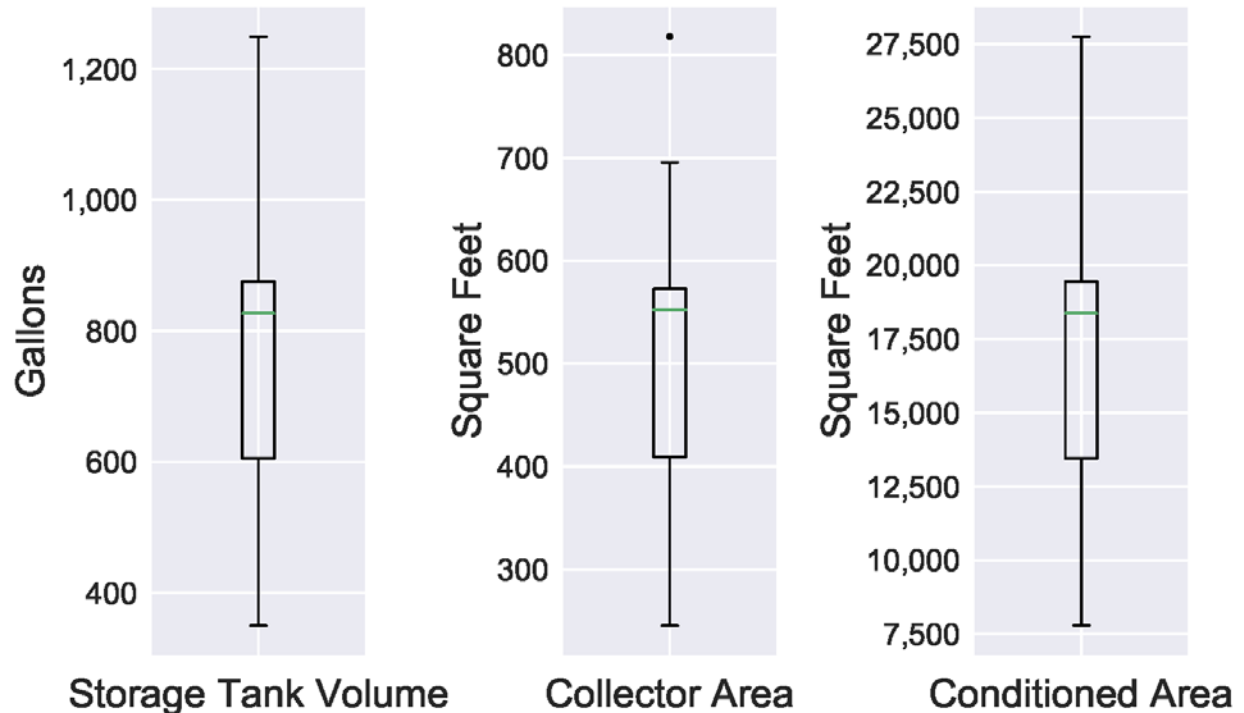
Figure 35. William Mead – Solar Fraction, Gas Consumption w/o SWH, and Gas Savings per Building



The histograms in Figure 35 show the distribution of solar fraction, gas consumption, and gas savings across the 24 structures on the 4 residential parcels that make up the William Mead Homes. Individual solar fractions for SWH systems range from approximately 30% to >90%. All

of the SWH systems meet the minimum performance requirement set by Title 24 (>20% average annual solar fraction).

Figure 36. William Mead – Collector Areas, Tank Volumes, and Conditioned Areas for SWH System Simulations.



The baseline assumptions for conditioned area and system sizing for William Mead produce the distribution of tank volume and collector area shown in Figure 36. Storage tanks range from 200 - 1600 gallons, and collector area from 250 - 818 ft². The collector area translates to 6 - 20 individual collector panels per building.

4.3.2 Typical Case – South Bay Gardens, Los Angeles, CA.

South Bay Gardens is a 124-unit senior living center located in South Los Angeles. The property is owned and operated by the Housing Authority of the County of Los Angeles (HACoLA), and features a centralized heating system, a community kitchen, and shared laundry facilities.

Figure 37. Location of South Bay Gardens Complex

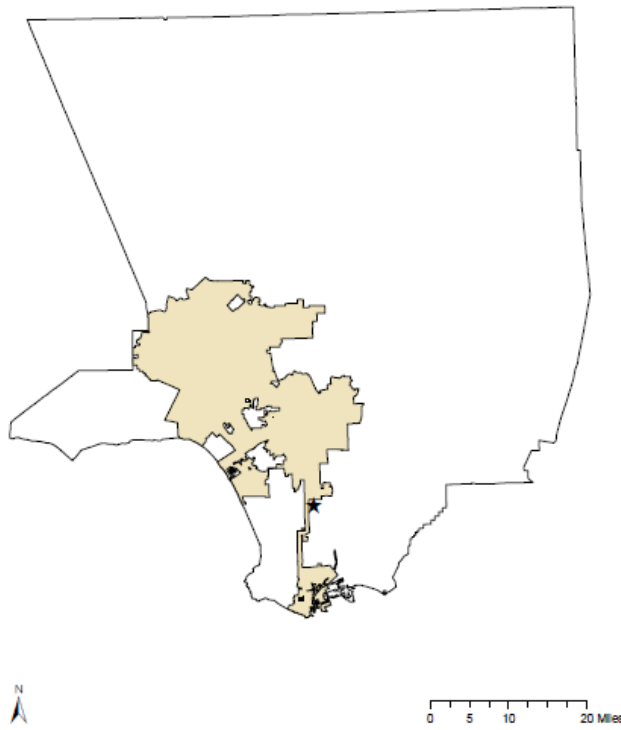


Figure 38. Aerial Images of South Bay Gardens





South Bay Gardens is located in the city of Compton due east of the I-10 Freeway.

Source: LARIAC/ EagleView, Inc.

South Bay Gardens represents a type of medium density development well-suited to community scale SWH. The site’s unobscured roof space, central boiler, and single, quasi-shared wall residential structure reduce retrofit costs.

Table 39. South Bay Gardens Site Data

Site Area	12920.5 m ²
Site Perimeter	506.28 m
Residential Units	124
Residential Structures	1
Current Water Heating Technology	Central Boiler
Additional Information	Senior living. Central laundry and kitchen facilities.

South Bay Gardens - Hot Water Demand and Conditioned Area Calculations

After several requests over two months, HACoLA representatives from the site and central administrative offices responded to requests for information about unit floorplans, building characteristics, and property ownership. As mentioned previously, South Bay Gardens is a

senior living center that provides meals, supportive services, and other amenities to residents, and the property is owned and maintained by Los Angeles County.¹⁵⁷

Table 40. South Bay Gardens - Hot Water Events & Event Frequencies

Event	Total Flow (120°F Draw-off)	Basis & Per Person Frequency
Food Preparation	3.96	1x Daily
Manual Dish Washing	3.96	1x Daily
Shower	3.96	1x Daily
Bath	15.85	1x Monthly
Face and Hand Washing	2.64	2x Daily
Clothes Washing	36.00	3x Monthly

South Bay Gardens’ 124 2-bedroom residential units are occupied by a maximum of two persons, who share a living room and kitchenette.¹⁵⁸ Regular meals are provided in the site’s cafeteria, thus only one manual dish washing event is assumed to occur per person per day. Each resident is assumed to generate 3 full loads of laundry per month. The conditioned area of South Bay Gardens is determined according to Equation 6.

South Bay Gardens’ hot water demand schedule implies the following monthly water and annual gas consumption per residential unit:

Table 41. South Bay Gardens - Calculated Water and Gas Consumption Values

Annual Gas Consumption per Residential Unit	2436.30 kWh/ 83.15 therm
Monthly Water Consumption per Residential Unit	1279.17 gal/ 1.71 HCF

Calculated water and gas consumption values for South Bay Gardens are below the median monthly water and annual gas consumption. However, both calculated consumption values meet the criteria listed in Section 1.2.1, and are within the interquartile ranges of their respective distributions. No further adjustment of the hot water demand schedule was necessary prior to system simulations. Distributions actual and water and gas consumption values for comparison come from properties with the following characteristics:

¹⁵⁷ Clarke, N. (5 July 2018). Personal Communication

¹⁵⁸ *Ibid.*

Table 42. South Bay Gardens - Comparison Property Sample Characteristics

Property Characteristics	Database Query Criteria
Construction Vintage	1950 - 1978
Parcel Square Footage	20,000 – 30,000 ft ²
Number of Res. Units	50 - 200 Units, Inclusive
Parcel Usetype	Multifamily

South Bay Gardens - System Design & Simulation Results

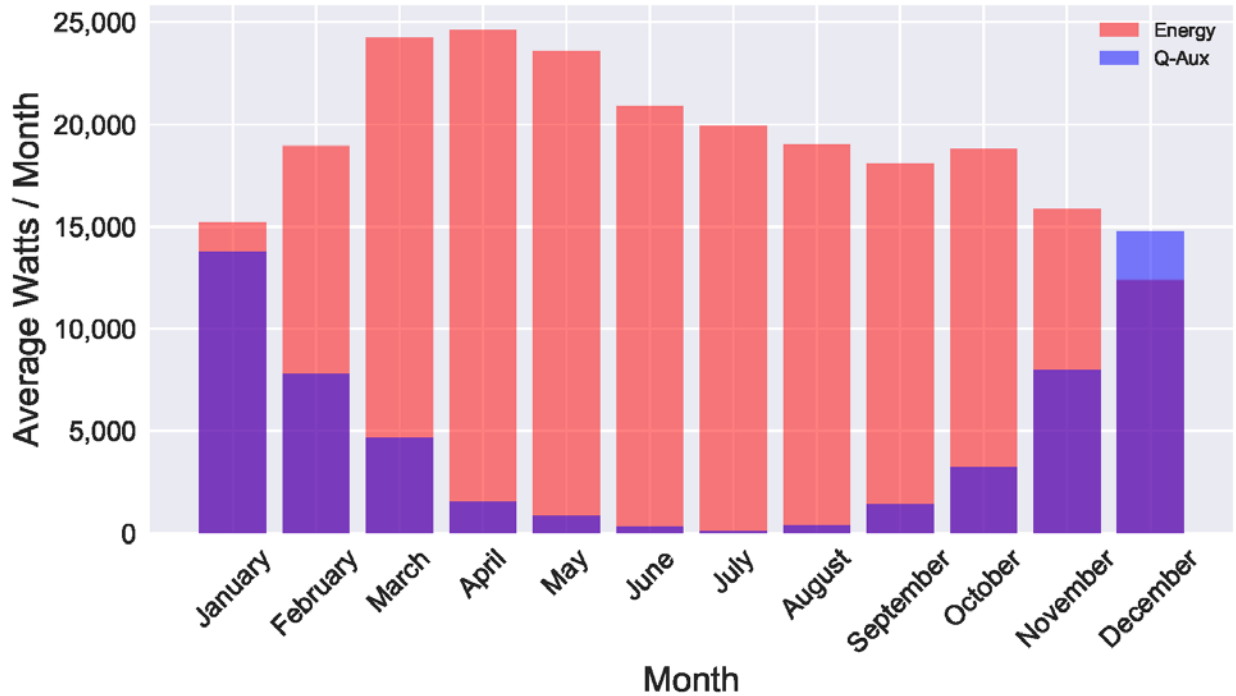
Simulation of South Bay Gardens' SWH system yields the following results:

Table 43. South Bay Gardens – Site Summary of SWH Simulation Results

Performance Metrics	Values
Average Annual System Energy	231552.91 kWh
Average Solar Fraction	0.8027 (80.3% solar energy for water heating)
Average Annual Heat Delivered	430885.97 kWh
Average Annual Auxiliary Heat Required w/ Solar	56885.56 kWh
Average Annual Heat Delivered - Auxiliary Only	2.886213e+05 kWh

South Bay Gardens' SWH system meets both Title 24 requirements and qualifies for the CSI-Thermal Performance Based Incentive. Due in part to its relatively low per unit hot water demand, South Bay Gardens has the highest annual solar fraction of the sites included in this study.

Figure 39. South Bay Gardens – Average Monthly SWH System Energy & Average Monthly Auxiliary Energy



According to the result of the simulation, South Bay Gardens’ SWH system should be able to meet almost all of the site’s hot water demand with solar energy during the months of June, July, and August.

Table 44. South Bay Gardens – Gas Consumption w/o SWH, and Gas Savings per Building.

Annual Gas Consumption w/o SWH System	481,035 kWh/ year
Gas Savings w/ SWH System	525, 470 kWh/ year

Table 44 shows the annual consumption of gas implied by the hot water demand schedule with and without the site’s SWH system. Table 45 shows the collector area, the number of collector panels, tank volume, and conditioned area for the site.

Table 45. South Bay Gardens – Collector Area, Tank Volume, and Conditioned Area for SWH System Simulation.

Collector Area	1065.63 ft ²
Collector Panels	99
Solar Tank Volume	6078.91 gals

Conditioned Area	135087 ft ²
------------------	------------------------

4.3.3 Typical Case – Crescent Court Apartment, Los Angeles, CA.

The Crescent Court Apartments is a multi-family HACLA property located in the MacArthur Park neighborhood of Los Angeles. The 2-bedroom units are designed to accommodate larger families.

Figure 40. Location of the Crescent Court Apartments

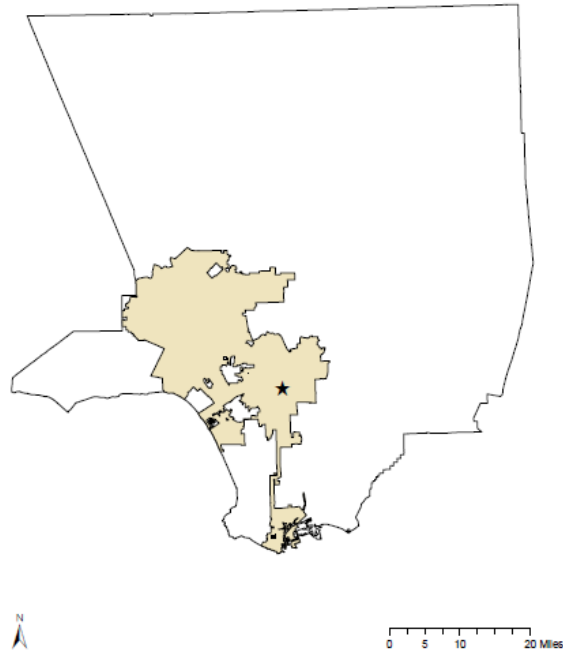
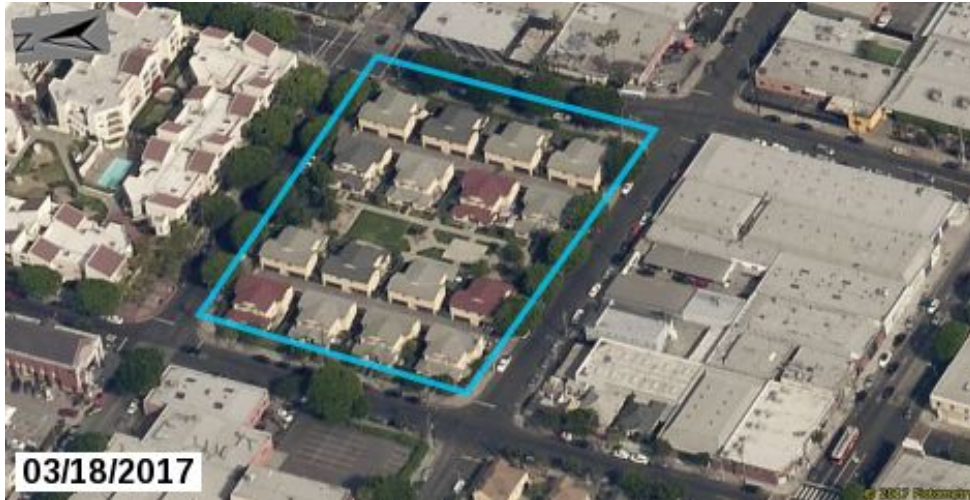


Figure 41. Aerial Images of the Crescent Court Apartments





The Crescent Court Apartments are located Northwest of Downtown Los Angeles.

Source: LARIAC/ EagleView, Inc.

The Crescent Court Apartments are poorly suited to SWH because of the inefficient use of the available space (two units per structure), and the pitched roofs of the apartment buildings. The apartment buildings are also separated by paved alleyways.

Table 44. Crescent Court Apartments Site Data

Site Area	8153.16 m ²
Site Perimeter	363.94 m
Residential Units	32
Residential Structures	16
Current Water Heating Technology	40-gal storage WH per unit
Additional Information	Multi-family. Dishwashers in all but 2 units, washing machines in all units.

Crescent Court - Hot Water Demand and Conditioned Area Calculations

HACLA representatives from the Public Housing Department responded to requests for information about unit floorplans, building characteristics, and property ownership about one month after an initial inquiry.¹⁵⁹ Maximum occupancy for the units, a list of hot water fixtures and appliances, and information the current hot water heating were provided.

¹⁵⁹ Maroutian, A. (12 June 2018). Personal Communication.

Table 45. Crescent Court - Hot Water Events & Event Frequencies

Event	Total Flow (120°F Draw-off)	Basis & Per Person Frequency
Food Preparation	3.96	1x Daily
Manual Dish Washing	3.96	1x Daily
Shower	3.96	1x Daily
Bath	15.85	1x Monthly
Face and Hand Washing	2.64	1x Daily
Dishwasher		3x Monthly
Clothes Washing	36.00	1x Monthly

Crescent Court’s 32 residential duplex units are rented to families with children, and have a maximum occupancy of 9 persons. All of Crescent Court’s units have a full kitchen, a washer-dryer, and two bathrooms. All but two of the units come with a dishwasher. No manual dishwashing is assumed to occur in units with dishwashers

Prior to simulation, the frequency of hot water events in Crescent Court’s demand schedule was altered so that monthly water consumption per unit met the <8 HCF per month criterion stipulated in Section 4.2.1. Crescent Court’s units are occupied by families, and it is unlikely that members of the household undertake food preparation, clothing and dish washing separately. For those two reasons, the frequency of the daily events and clothes washing has been set to 1. These changes brought down monthly per unit water consumption below the 8 HCF limit.

Following South Bay Gardens’ hot water demand schedule implies the following monthly water and annual gas consumption per residential unit:

Table 46. Crescent Court - Calculated Water and Gas Consumption Values

Annual Gas Consumption per Residential Unit	7612.17 kWh/ 259.80 therm
Monthly Water Consumption per Residential Unit	3343.79 gal/ 4.47 HCF

Calculated water and gas consumption values for Crescent Court are very close to the 4th quartile of their respective distributions. Crescent Court’s relatively high hot water demand is consonant with ASHRAE and ASPE’s observations that families with children consume, on

average, more hot water per person per day than other domestic arrangements.^{160, 161} Following the frequency adjustment described above, Crescent Court’s calculated consumption values met the criteria listed in Section 4.2.1. Distributions actual and water and gas consumption values for comparison come from properties with the following characteristics:

Table 47. Crescent Court - Comparison Property Sample Characteristics

Property Characteristics	Database Query Criteria
Construction Vintage	1950 - 1978
Parcel Square Footage	10,000 – 20,000 ft ²
Number of Res. Units	20 - 50 Units, Inclusive
Parcel Usetype	Multifamily

Crescent Court - System Design & Simulation Results

Unlike the other case study sites included in this study, Crescent Court’s SWH systems did not achieve the 20% minimum performance standard set forth in Title 24 when sized with the ratios listed in Table 2, and thus did not qualify for the CSI-Thermal Performance Based Incentive. Given that SWH retrofits must qualify for the CSI-Thermal PBI to make financial sense for property owners, Crescent Court’s SWH system parameters had to be altered and their simulations re-run.^{162, 163}

There are numerous ways to increase the performance (i.e. solar fraction) of a SWH system. In this case, one additional collector was added to the number of panels calculated using the ratios in Table 2. This change yielded individual solar fractions between 21-28% for each of the 16 buildings.

Table 48. Crescent Court – Site Summary of SWH Simulation Results w/ 1 Additional Collector per SWH

Performance Metrics	Values
Average Annual System Energy	12678.33 kWh
Average Solar Fraction	0.2653 (26.5% solar energy for water heating)
Average Annual Heat Delivered	12857.65 kWh

¹⁶⁰ Kalogirou, S. A. (2013). Solar energy engineering: processes and systems. Academic Press.

¹⁶¹ ASPE. (2015). CEU22 – Domestic Hot Water Systems – Continuing Education from the American Society of Plumbing Engineers. Retrieved from: https://www.aspe.org/sites/default/files/webfm/ContinuingEd/CEU_221_Mar15.pdf

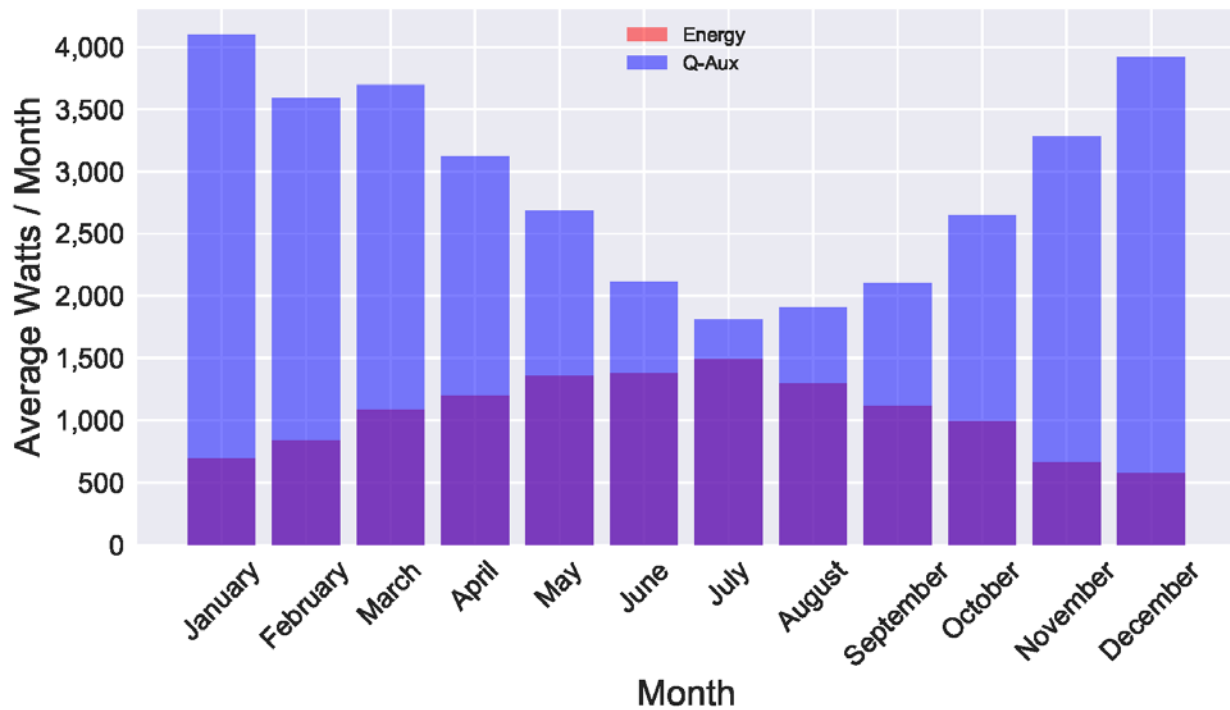
¹⁶² Chen, W. (10 July 2018). Personal Communication.

¹⁶³ Clarke, N. (5 July 2018). Personal Communication.

Average Annual Auxiliary Heat Required w/ Solar	34964.545 kWh
Average Annual Heat Delivered - Auxiliary Only	4.779490e+04 kWh

With the 1 additional collector per system, Crescent Court now meets both Title 24 requirements and qualifies for the CSI-Thermal Performance Based Incentive. However, Crescent Court has the lowest average annual solar fraction of any of the systems simulated in this study. The low solar fraction of Crescent Court’s SWH systems is due in part to the high per unit hot water demand.

Figure 42. Crescent Court – Average Monthly SWH System Energy & Average Monthly Auxiliary Energy with 1 Additional Collector per System



Like the other systems simulated in this study, Crescent Court’s solar fraction is highest in the summer and lowest in the winter, varying from approximately 80% in July to 12-15% in December/ January.

Figure 43. Crescent Court – Solar Fraction, Gas Consumption w/o SWH, and Gas Savings per Building.

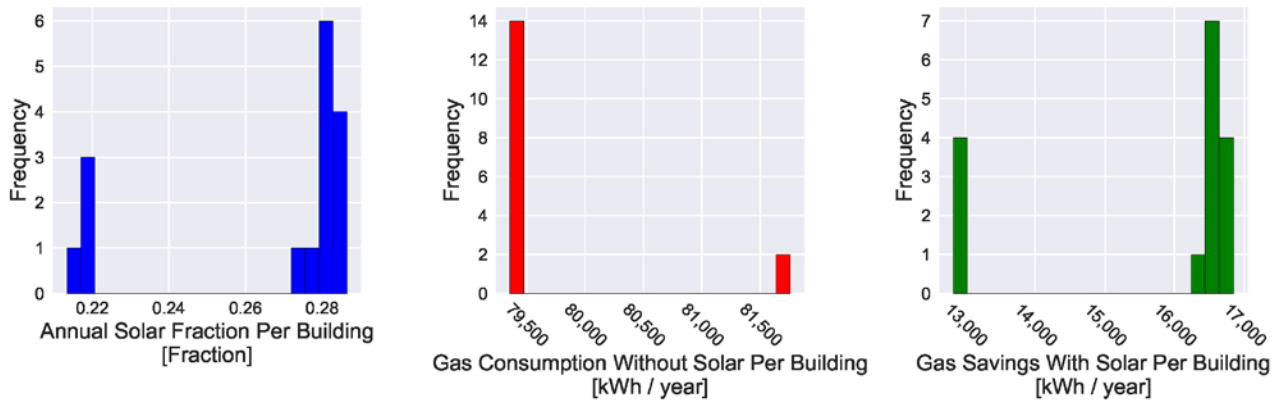
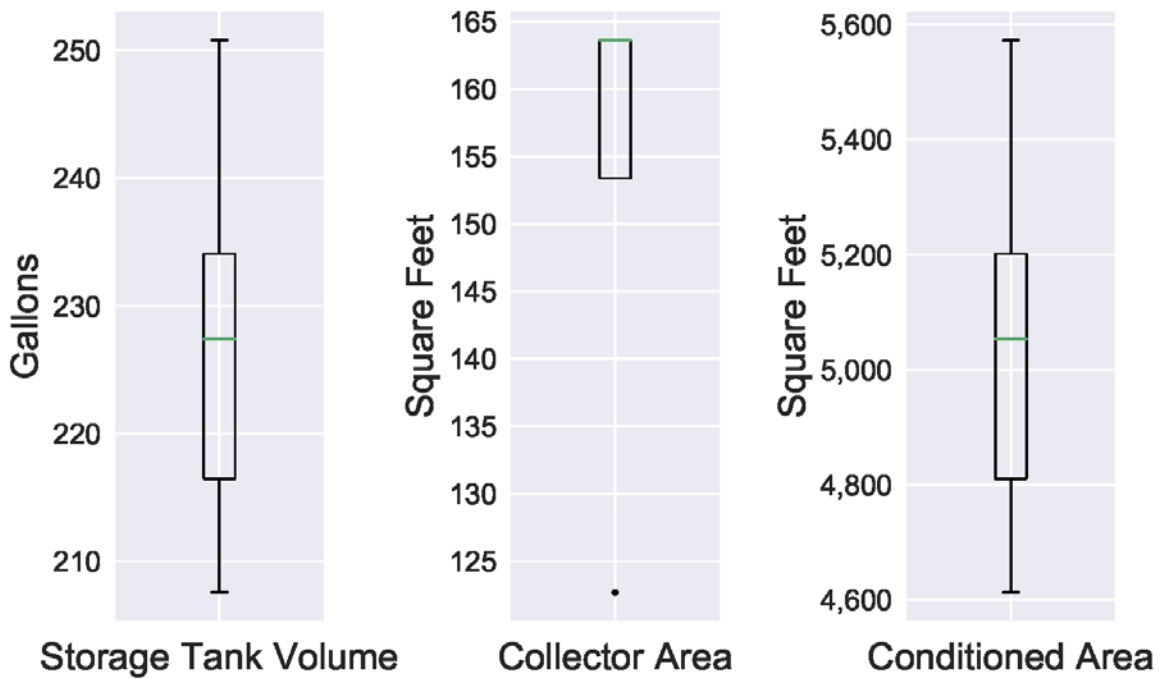


Figure 26 shows the annual consumption of gas implied by the hot water demand schedule with and without the site's SWH system. Figure 27 shows the distributions of collector area, tank volume, and conditioned areas for each of Crescent Court's buildings.

Figure 44. South Bay Gardens – Collector Area, Tank Volume, and Conditioned Area for SWH System Simulation.



Chapter 5: Analysis of Simulation Results & Policy Implications

5.1 Influence of Site Characteristics on System Performance

Based on the simulation results presented in Chapter 4, it is possible to draw conclusions about how site characteristics affect the performance of community scale SWH systems similar to those studied here (active, closed systems w/ flat plate collectors). It should be noted that the results of the simulations depend on the assumptions about thermal energy transfer and efficiency implicit in the SAM SWH module, and are sensitive to changes in the assumed volume and delivery schedules of hot water demand.¹⁶⁴ Therefore, relationships observed between site characteristics and system performance should be understood as preliminary findings. The relationships discussed here are suitable subjects for future modeling/ simulation studies.

5.1.1 Roof Area to Conditioned Area Ratio

Given the value and scarcity of open space on residential parcels, SWH systems installed in Los Angeles County will, in most instances, have their collector arrays located on building rooftops. This means that residential structures for which community scale SWH is feasible must, in addition to the general feasibility criteria, also have sufficient rooftop space to accommodate the system's collector array.

Pacific Plaza illustrates how some forms of residential development with low roof area to conditioned area ratios (in this case, high-rise apartment complexes) are not especially well-suited to community scale SWH. Using the Title 24 SWH system sizing ratios, the conditioned area for the site (100,201 ft²) implies a collector area of 9,034 ft², or approximately 221 4' x 10' flat plate collectors. Pacific Plaza's gross rooftop space, as measured using aerial LiDAR is 16,164 ft², which is apparently sufficient for the collector array. However, oblique aerial photos of the building's roof show that the roof space on which collector arrays could be installed is considerably less than the gross area.

¹⁶⁴ Diorio, N., Christensen, C., Burch, J., & Dobos, A. (2014). Technical Manual for the SAM Solar Water Heating Model. Retrieved from https://sam.nrel.gov/system/tdf/SimpleSolarWaterHeatingModel_SAM_0.pdf?file=1&type=node&id=69521

Figure 45. Rooftop of Pacific Plaza Building



A low rooftop to conditioned area ratio makes the siting of collector arrays more difficult, and, assuming that putative systems are similar to those considered in this study, appears to constrain the performance of SWH systems. Pacific Plaza has the lowest annual site solar fraction (28.1%) of the three private cases studied, and features the second lowest performing system out of all the simulations performed (of the 102 individual buildings on the six sites). Twenty-eight percent is also likely an over-estimate of Pacific Plaza's annual solar fraction. NREL SAM's SWH simulation method does not account for the additional grid-supplied energy required to pump water against gravity to solar tanks on floors with residential units.

The Pacific Plaza case illustrates how the development of distributed solar energy systems and urban densification efforts can, in certain instances, conflict with one another. This notion will be discussed in further detail in Section 4, but *for community scale solar thermal systems, the limited rooftop space of high-rise, high-density housing developments constrains the collector area, limiting system performance. Building upwards also complicates construction of community scale SWH systems in retrofit cases, and increases the amount of energy required to pump both potable water and heated working fluid to solar storage tanks.*

5.1.2 Residential Density & System Performance

Another important influence on system performance is the 'population density' of the units in a residential building and demographics of current or putative occupants. Comparison of simulation results between the public cases shows that for buildings with high-density units and high hot water demand demographic types (families with children, for example) the Title 24 system sizing ratios may not yield a SWH system that qualifies for the applicable incentives. Conversely, for buildings with low population densities and low hot water demand demographic types (adults w/o children, seniors) smaller systems may suffice, assuming they can still meet the performance requirements for incentive programs.

Crescent Courts is illustrative of a high-density, high-demand case. In this instance, the Title 24 sizing ratios do not yield systems that meet the minimum performance requirement for the CSI-Thermal incentive. According to HACLA, the Crescent Courts development is intended to house families with children, and each unit has a maximum occupancy of 9 persons (each unit is identical to the others).¹⁶⁵⁻¹⁶⁶ This is considerably higher than average occupancy per unit of the William Mead Homes (3.76 persons per unit), the other public housing site intended for families. Simulations for Crescent Court using the hot water demand schedule in Table 22, and the Title 24 system sizing ratios yielded annual solar fractions below the CSI-Thermal performance threshold for the climate zone (20% average annual solar fraction). In order to meet the 20% requirement, it was necessary to add one additional collector to each system on the Crescent Court site. In subsequent simulations with the additional collectors, each of Crescent Court's SWH systems met or exceeded the CSI-Thermal performance requirement.

South Bay Gardens, a supportive senior living center with an average per unit occupancy of 2 persons, represents a low-density, low-demand case. Residents do not do their laundry or prepare their own meals since the site features central laundry and kitchen facilities (some units have kitchenettes). The average per unit occupancy is also the lowest of the three public cases. Simulations using the hot water demand schedule in Table 22 and system parameters derived from the Title 24 sizing ratios yielded an annual solar fraction of 80%, the highest annual solar fraction of all of the sites studied. The simulation results suggest that for residential sites like South Bay Gardens, a smaller, less materially intensive community scale SWH system may be economically optimal. Overbuilt SWH systems use a greater portion of the site's rooftop space and, depending on the price of auxiliary energy, will in most instances have longer payback periods.

The population density of residential units and the demographic profile of their inhabitants determine the hot water demand and consumption patterns.¹⁶⁷ ***In order to design a community scale SWH system that is optimally sized, configured, and operated, as much as possible needs to be known about the current or potential inhabitants of the building served by the system.***¹⁶⁸ ***Changes in occupancy levels or the demographics of residents can dramatically alter demands on building level SWH systems.***

5.1.3 Returns to Scale for SWH System Performance

One of the questions that motivated the study of community scale solar water heating is the possibility that larger systems may be able to achieve superior performance by virtue of their

¹⁶⁵ Marouthian, A. (12 June 2018). Personal Communication.

¹⁶⁶ Housing Authority of the City of Los Angeles. (2018). *About Public Housing*. Retrieved from: <http://home.hacla.org/aboutpublichousing>

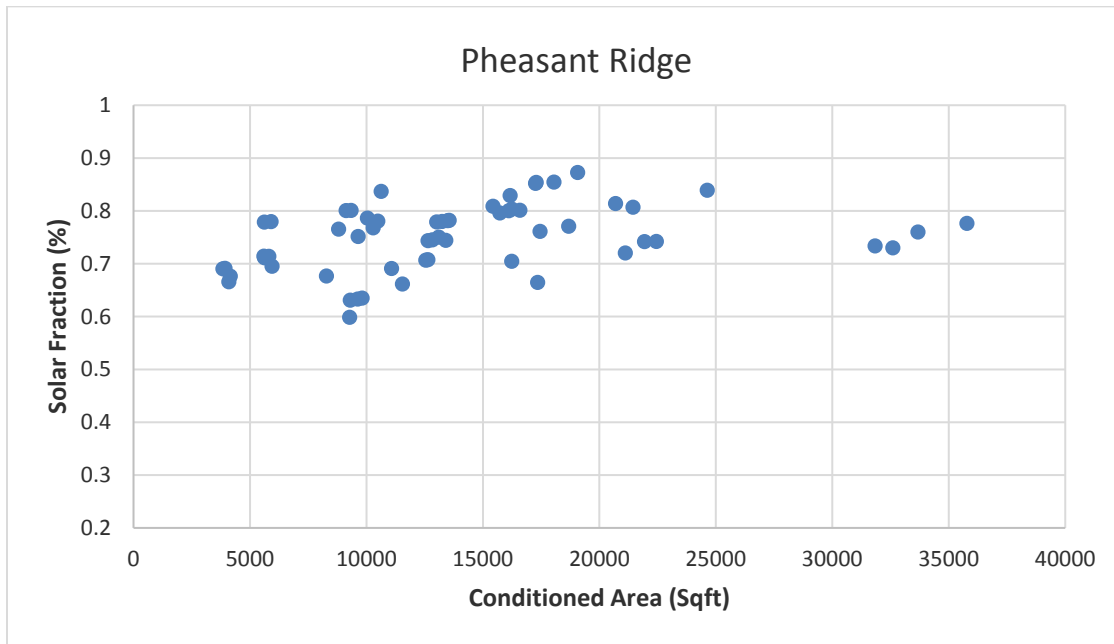
¹⁶⁷ Bertrand, A., Mastrucci, A., Schüler, N., Aggoune, R., & Maréchal, F. (2017). Characterization of domestic hot water end-uses for integrated urban thermal energy assessment and optimization. *Applied Energy*, 186, 152-166. <https://doi.org/10.1016/j.apenergy.2016.02.107>

¹⁶⁸ Fuentes, E., Arce, L., & Salom, J. (2018). A review of domestic hot water consumption profiles for application in systems and buildings energy performance analysis. *Renewable and Sustainable Energy Reviews*, 81(February 2017), 1530-1547. <https://doi.org/10.1016/j.rser.2017.05.229>

centralized design and large heat storage tanks.¹⁶⁹ While the question of how the efficiency and performance of centralized, parcel-scale systems compare to structure-scale systems is not addressed here, the case studies provide some insight into how different measures of system ‘size’, such as building occupancy and conditioned area, affect the performance of community scale SWH systems.

As mentioned in Section 1.1.2, the conditioned area of a building is the area of the inhabited floor space. Conditioned area is estimated from the LARIAC building outlines dataset and, in some cases, orthogonal aerial imagery of the sites.¹⁷⁰

Figure 46: Conditioned Area vs. Solar Fraction for Sites with Multiple Buildings



¹⁶⁹ U.S. Army Corps of Engineers. (1 December 2011). *Central Solar Hot Water Systems Design Guide*. Retrieved from: <https://www.wbdg.org/ffc/army-coe/design-guides/central-solar-hot-water-systems-design-guide>

¹⁷⁰ Los Angeles Regional Imagery Acquisition Consortium. (2016). *LARIAC 5* [dataset and photographs]. EagleView/ Pictometry Inc.

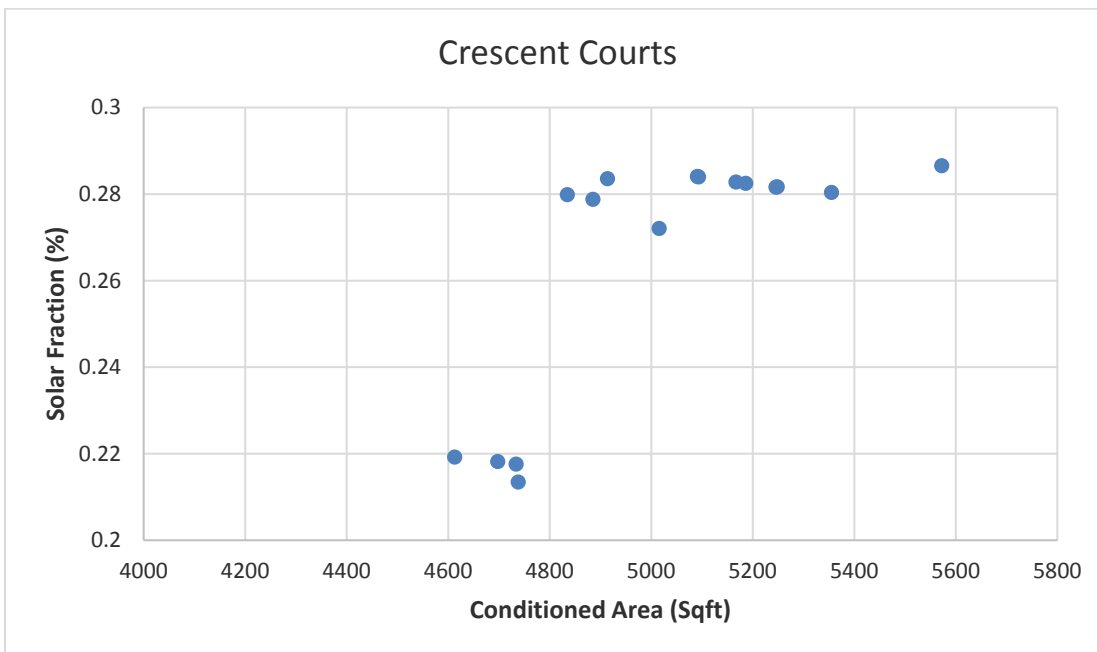
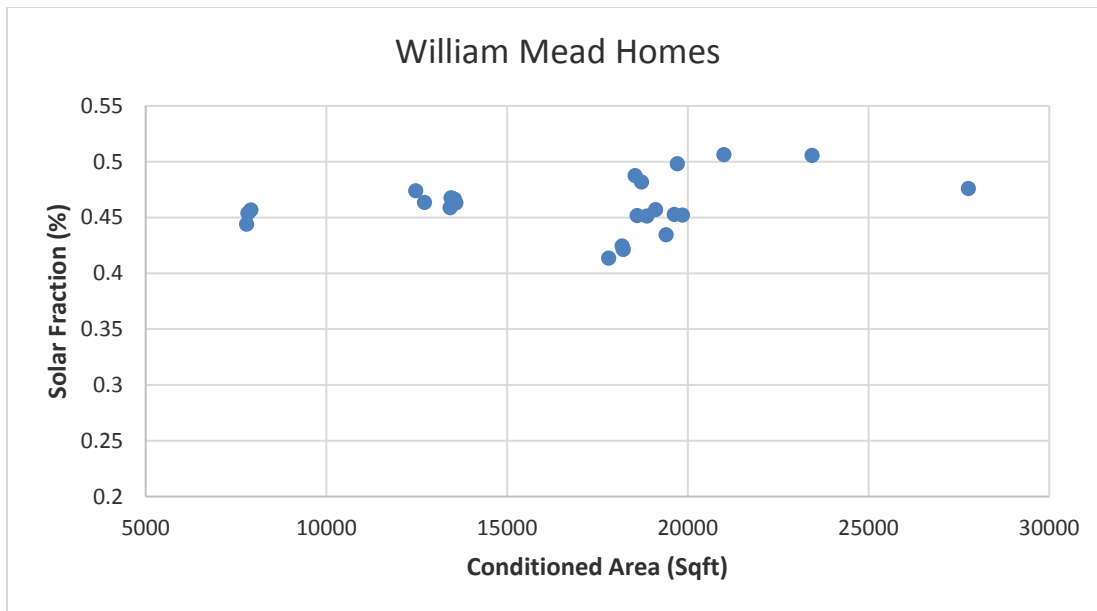


Figure 29 shows the relationship between the conditioned areas and annual solar fractions for the three sites with more than one building. For the range of conditioned areas observed (and simulation method employed) in this study, systems sized according to the Title 24 ratios display fairly consistent performance, the only exception being Crescent Courts.

Pheasant Ridge has the greatest difference between the best and worst performing systems on site (27.4%). This range in solar fraction is attributable to the site's heterogeneous unit floorplans. The floorplans determine the maximum occupancy and the set of possible end uses for hot water for a unit, and thus the volume of demand.

William Mead is a more homogeneous with respect to unit floorplan, and displays smaller range of annual solar fractions for its structures (10%). Crescent Courts, the site with the most homogeneous structures (duplexes with nearly identical layouts and amenities) is the most homogeneous of the sites with multiple structures, and displays the smallest range of solar fractions (7%). The difference between the two distinct clusters of points in Crescent Court’s scatterplot is attributable to the absence of dishwashers in two of the site’s buildings.

Conditioned area is a proxy for the population density of a residential structure, which is in turn a proxy for hot water demand. *Situations in which the maximum occupancy to conditioned area ratio of a residential structure deviates considerably from the normal range may require special consideration. The results of the case studies show that the sizing ratios can yield systems that perform well and qualify for relevant incentives, but for large, sparsely inhabited buildings (Pacific Plaza) and small, densely inhabited buildings (Crescent Courts), sizing systems with conditioned area ratios may lead to sub-optimal system performance.*

5.2 Community Scale Solar Water Heating Suitability Criteria for Existing Residential Developments

As discussed previously, the six case study sites were selected based on their SWH suitability scores and representativeness of different residential development patterns common in LA County (see the *Case Study Site Selection Report* for a full discussion of selection). The selection criteria used, namely the suitability scores for residential parcels, were developed based on observed, empirical relationships between urban form and SWH system performance, and refined with expert assistance.¹⁷¹⁻¹⁷²⁻¹⁷³ The results of the simulations show that, for the cases considered, parcel suitability score was at least somewhat predictive of system performance. Table 26 summarizes site ranking and performance:

Table 49. Suitability Score Categories and Solar Fractions for Case Study Sites

Performance Ranking	Case Study Site	Suitability Score Quintile	Solar Fraction Mean ($\pm \sigma$, n = number of buildings)
1	South Bay Gardens	Typical	80.2 % (n = 1)
2	Pheasant Ridge Apartments	Well-Suited	75% \pm 6% (n = 59)
3	William Mead	Well-Suited	46.1% \pm 2.4%

¹⁷¹ Chen, W. (10 June 2018). Personal Communication.

¹⁷² Kalogirou, S. A. (2013). Solar energy engineering: processes and systems. Academic Press.

¹⁷³ Anderson, K. (10 June 2018). Personal Communication.

			(n = 24)
4	Promenade Apartments	Typical	45.3% (n = 1)
5	Pacific Plaza	Poorly-Suited	28.1% (n = 1)
6	Crescent Courts	Poorly-Suited	26.5% ± 2.8% (n = 16)

The solar water heating suitability score developed for the purpose of this study awards densely constructed and populated parcels with contiguous structures with higher scores, and less dense parcels with more diffuse and irregular development patterns lower ones. Higher scores indicate greater suitability for community scale SWH. The suitability score metric was used to partition the pools of candidate parcels into categories from which individual cases were selected. *The discrepancies between the suitability category designations and the results of the simulations suggest that a more comprehensive set of building and parcel characteristics is needed to determine the suitability of a residential structure or development for community scale SWH. The results of case study simulations indicate that densely constructed and inhabited buildings are better for community scale SWH to the extent that they have sufficient rooftop space for collector arrays, and do not have especially high or low maximum occupancies per unit conditioned area.*

A county-wide using non-linear regression methods to elucidate the relationships between resident demographics, building characteristics, and the Energy Atlas's gas consumption data would provide a ranked list of variables that influence a residential parcel's suitability for community scale solar water heating.

5.3 Financial Considerations for Community Scale Solar Water Heating

Interviews with solar engineers and contractors, housing authority officials, incentive program administrators, and suppliers of system components yielded a great deal of information about how building-scale solar thermal systems are financed, the cost drivers for SWH projects, and the decision landscapes facing public and private property owners. The following sections describe the decision landscapes faced by the three types of property owners (private, private nonprofit, and public), drawing upon the information gathered from the case studies and interviews.

5.3.1 Financial Considerations for Privately Owned Properties

Of the three types of developments included in this report, privately owned residential properties are the easiest to retrofit with community scale SWH systems. Owners of residential

developments also have the greatest incentive to install high-performing community-scale systems of the three types of property owners.

Building-scale systems installed on privately owned residential properties are eligible for the CSI-Thermal rebate and the federal Residential Renewable Energy Tax Credit:^{174, 175}

Table 50. Applicable Incentives for Community Scale SWH – Private Residential

	Applicable Incentives	Incentive Structure	
Private Residential Owners	CSI-Thermal - Multifamily Residential or Commercial	Performance-based: minimum SF = 20%	\$20.19 per therm of annual energy savings
	Residential Renewable Energy Tax Credit	Cost-based: minimum SF = 50%	30% of qualified capital expenditures for systems installed by 12/31/2019.

In practice, SWH systems installed on private properties in LA County are designed to be eligible for the CSI-Thermal Rebate and the Residential Renewable Tax Credit, as solar water heating is not competitive with natural gas on a cost basis without the incentives described in Table 27.^{176, 177} Therefore all community scale SWH systems installed on privately owned property will be designed to have solar fractions of at least 50%. In interviews, solar contractors, suppliers of component technologies, and engineers who design systems for residential and commercial buildings all emphasized that SWH systems of the type considered here are relatively straightforward to scale up, but that ensuring no disruption of hot water service occurs for large centralized systems (i.e. a single system serving hundreds of units in a large apartment building) in the event of malfunction can incur additional costs and complicate construction.¹⁷⁸

Incentives for SWH systems apply most naturally to sites with a single structure. The Residential Renewable Energy Tax Credit requires that the property owner be able to claim the property as a residence.¹⁷⁹ Furthermore, qualification for the applicable incentives, and the calculations of incentive totals are more complicated for community-scale systems installed on properties with multiple residential buildings due to the language of the eligibility requirements.

¹⁷⁴ California Public Utilities Commission. (May 2018). *California Solar Initiative-Thermal Program Handbook*. Retrieved from: <https://www.csithermal.com/tracker/>

¹⁷⁵ U.S. Department of Energy. (2018). *Residential Renewable Energy Tax Credit*. Retrieved from: <https://www.energy.gov/savings/residential-renewable-energy-tax-credit>

¹⁷⁶ Bavin, T. (7 July 2018). Personal Communication.

¹⁷⁷ Chrisman, Adam. (29 May 2018). Personal Communication.

¹⁷⁸ *Ibid.*

¹⁷⁹ U.S. Department of Energy. (2018). *Residential Renewable Energy Tax Credit*. Retrieved from: <https://www.energy.gov/savings/residential-renewable-energy-tax-credit>

5.3.2 Financial Considerations for Properties Owned by Private Nonprofit Entities

Private nonprofit housing organizations, such as National CORE, the owners of Promenade Apartments, provide below-market housing and supportive services to vulnerable populations in Los Angeles County. ***Private nonprofit housing organizations own a relatively small share of the residential housing stock, but they provide vital services to their clients, and advocate for affordability, environmental justice, and against discriminatory housing practices.***¹⁸⁰ ***Thus, consideration should be given to the ease with which private nonprofit housing organizations can realize opportunities for reducing their properties' energy consumption through the development of community scale SWH systems.***

Retrofitting buildings for community scale SWH is a more expensive proposition for housing nonprofit organizations than it is for private property owners. Nonprofits may take advantage of the CSI-Thermal incentive, but not the federal Residential Renewable Energy Tax Credit. The Residential Renewable Energy Tax Credit cannot be claimed by private housing nonprofits because of their legal status as nonprofit organizations. However, most private housing organizations that rent to low-income citizens in LA County will qualify for an increased CSI-Thermal rebate incentive rate.¹⁸¹

Table 51: Applicable Incentives for Community Scale SWH – Private Nonprofit

	Applicable Incentives	Incentive Structure	
Private Nonprofit Residential Housing Organizations	CSI-Thermal Rebate – Multifamily Low-Income	Performance-Based: Minimum SF = 20%	\$24.98 per therm of energy savings

For example, Promenade Apartments, which is owned and managed by National CORE, requires a system with a minimum solar fraction of 20% to qualify for the applicable incentives. A system sized with the estimated conditioned area and Title 24 ratios yields an estimated annual solar fraction of 45.3%. Private nonprofit property owners therefore have an incentive to install community scale SWH systems that maximize possible solar fraction and minimize capital cost. ***Since no capital cost rebate is available to private nonprofits, they must be able to bear the capital costs of until the system is operational, at which point they can begin receiving rebate payments.***

5.3.3 Financial Considerations for Publicly Owned and Managed Properties

¹⁸⁰ Southern California Association of Non Profit Housing. (2018). *About Us - Mission*. Retrieved from: <http://www.scanph.org/mission>

¹⁸¹ California Public Utilities Commission. (May 2018). *California Solar Initiative-Thermal Program Handbook*. Retrieved from: <https://www.csithermal.com/tracker/>

HACLA and HAcOLA’s public housing developments are occupied by thousands of County residents who are unable to find suitable or affordable accommodations on the private market. The City and County housing authorities must provide safe and livable conditions for residents, and ensure that their housing stock keeps pace with state and local energy efficiency goals and standards. Both organizations wish to lead by example with regard to sustainability and energy efficiency, and community scale SWH is one of a number of possible investments that the authorities could make to reduce their energy consumption.

Public housing is the most expensive type of property to retrofit with community scale SWH. There are three factors which drive up the cost of energy retrofits for public housing: Department of Housing and Urban Development rules governing the installation of renewable energy systems on properties under its jurisdiction, higher labor costs for public work contracts, and the fact that public housing does not qualify for the Residential renewable energy tax credit.¹⁸² However, public housing developments do qualify for the CSI-Thermal Low-Income rate.

Table 52. Applicable Incentives for Community Scale SWH – Public Housing

	Applicable Incentives		Incentive Structure
Public Housing Authorities	CSI-Thermal Rebate – Multifamily Low-Income	Performance-Based: Minimum SF = 20%	\$24.98 per therm of energy savings

HAcOLA’s installation of building-scale solar water heating systems at the Nueva Maravilla Housing Community illustrates how complex and expensive public SWH projects can be. Constructed in the 1930s, and renovated in the 1970s, Nueva Maravilla is one of the largest HAcOLA developments, and like William Mead and Crescent Courts, serves mostly families with children.

¹⁸² Clarke, Norma C. (11 July 2018). Personal Communication

Figure 47. Nueva Maravilla Housing Community Aerial Photos



Source: LARIAC/ EagleView, Inc.

In 2009, HCoLA won a \$5,000,000 federal grant to improve Nueva Maravilla. Between 2009 and 2013 the housing authority completed a series of site upgrades, including xeriscaping measures, energy-efficient exterior lighting, solar photovoltaic cells, and solar water heating systems (see Figure 30). The entire slate of improvements cost approximately \$12,000,000, and involved five private contractors in addition to HUD and HCoLA.^{183, 184}

HCoLA had originally intended to retrofit all 58 buildings on the Nueva Maravilla site with solar water heating systems, but ultimately decided to install systems on only 6 buildings because of provisions in HUD's Energy Performance Contracting Policy (EPC).¹⁸⁵ Prior to the start of improvement project, HCoLA had determined internally that the CSI-Thermal rebate was generous enough to warrant installing solar thermal systems on all of the buildings, but eventually abandoned this plan when confronted with the cost of the perspective studies and monitoring required by the EPC.¹⁸⁶ HUD's EPC requires that public housing authorities pay energy consultancies selected from pre-approved lists of firms to conduct prospective studies of renewable energy projects, and file annual observation and monitoring reports for the years after the projects are completed.^{187, 188} In the case of Nueva Maravilla's six solar thermal water heating systems, the prospective report cost HCoLA \$300,000, and the observation and monitoring reports an additional \$30,000 per year.¹⁸⁹ HCoLA claims that the consulting fees incurred by a site-wide retrofit would have outweighed the benefits of the estimated energy savings and rebate payments.¹⁹⁰

Unlike private and private nonprofit property owners, housing authorities cannot negotiate directly with solar thermal contractors. They must also pay for expensive estimates of system performance and ongoing monitoring.¹⁹¹ Combined with prevailing-wage requirements for system installation contracts, and the absence of other incentives to offset capital costs, community scale SWH is an expensive proposition for the public housing authorities in Los Angeles County, even if the chosen sites are well-suited for SWH retrofits.

¹⁸³ Ibid.

¹⁸⁴ HCoLA. (23 July 2013). County Housing Authority Receives Recognition for its Energy Efficiency Upgrades [press release]. Retrieved from: <https://www.hud.gov/sites/documents/PR-NUEVA-MARAVILLA-EPC.PDF>

¹⁸⁵ Clarke, Norma C. (11 July 2018). Personal Communication

¹⁸⁶ Ibid.

¹⁸⁷ Ibid.

¹⁸⁸ U.S. Department of Housing and Urban Development. (2018). Public Housing Energy Conservation Clearinghouse: Energy Performance Contracting.

¹⁸⁹ Clarke, Norma C. (11 July 2018). Personal Communication

¹⁹⁰ Ibid.

¹⁹¹ Chen, W. (7 July 2018). Personal Communication.

5.4 Policy Implications

The case studies demonstrate that community scale SWH can displace ~20-80% of the gas required for domestic water heating, depending on building-level characteristics and the demographics of the site's residents. Community scale systems can be constructed from the components used to build single-family and commercial scale systems, and in all but one case (Crescent Courts), the systems simulated in this study did not require exception from sizing guidelines and residential building code. Community scale solar water heating systems, of the kind considered in this study, can significantly reduce the amount of natural gas consumed for domestic water heating. However, the case studies also indicate that the performance of a given community scale SWH system is sensitive to the population density of the structure it serves. In extreme cases (i.e. large, sparsely populated buildings and small, densely populated ones), the conditioned area to storage volume, and collector area to storage volume ratios used to programmatically size systems may fail to yield adequate solar fraction.

Community scale solar water heating is a viable approach to reducing demand for natural gas, but questions remain about where the technology could be deployed most beneficially. To understand the role community scale solar thermal could play in reducing energy consumption and emissions from LA County's residential housing sector, it is essential to consider how this technology interacts with other sustainability initiatives:

5.4.1 Implications for Densification Efforts in LA County

Zoning, land use changes, and specific plans for denser residential development have been proposed by public stakeholders as a solution to LA County's housing shortage, congestion issues, and as part of broader sustainability initiatives.¹⁹²⁻¹⁹³ If densification efforts achieve their intended effect, population centers in the County will transition away from single-family homes and duplexes towards larger multi-story apartment buildings and mixed-use developments. These denser developments, to the extent that they have sufficient rooftop space, may be suitable for a community scale approach to solar water heating. Structures similar to those in top three cases (Pheasant Ridge, South Bay Gardens, and William Mead) are examples of densely inhabited residential buildings that are suitable for community scale SWH. Buildings on these sites are 2-3 stories and have residential unit occupancies of 2-8 persons.

Pacific Plaza illustrates how densification efforts can potentially conflict with the installation and operation of solar thermal systems. Building upwards complicates the installation of solar thermal systems, while diminishing rooftop area to conditioned area ratio constrains the performance of putative SWH systems. In Pacific Plaza's case, limited rooftop space and Title 24 building code requirements make the rooftop placement of the 221 collector panels required for the system virtually impossible. There are two possible solutions to the problem of limited rooftop space. First, systems on high-rise buildings could use collector technologies capable delivering more energy per unit collector area than flat-plate panels, such as evacuated tube collectors or concentrating solar collectors. Second, in cases where the vertical aspects of a

¹⁹² Los Angeles Department of City Planning. (2017). *Expo Corridor Transit Neighborhood Plan*. Retrieved from: <http://www.latnp.org/expo-line/expo-draft-plan/>

¹⁹³ The NOW Institute. (2016). *99% Preservation, 1% Densification: A case for 2050 sustainability through a denser, more connected Los Angeles*. Retrieved from: <https://grandchallenges.ucla.edu/happenings/2016/10/24/the-now-institute-and-sustainable-la-grand-challenge-launch-visions-for-a-sustainable-la/>

structure are sufficiently exposed, collector capacity can be installed as a façade. However, both of these solutions would require special consideration under Title 24.

5.4.2 Implications for Proliferation Distributed Solar Energy Systems & Potential as an Emissions Reduction Technology

Community scale SWH is fundamentally different from other alternatives for reducing the carbon intensity of residential water heating (heat pumps, high-efficiency boilers, demand reduction, and appliance efficiency standards) in that it competes for rooftop space with solar PV. Rooftop space is becoming an increasingly valuable (and limited) resource in Los Angeles County; incipient building code changes will require that new residential structures under three stories install PV cells and that other classes of structure be built to accommodate PV installation in the future.¹⁹⁴ The forthcoming changes to Title 24 will alter the decision landscape for property developers who may be considering SWH as a way to reduce natural gas consumption, and introduce logistical challenges that are not well-studied, and for which ready solutions do not yet exist.¹⁹⁵ More work is necessary to establish how limited rooftop space can be best used to meet residential demand for thermal and electrical energy.

How solar thermal and photovoltaic capacity can be optimally deployed to provide the maximum amount of renewable energy (thermal and electrical) is an open question in engineering research.¹⁹⁶⁻¹⁹⁷⁻¹⁹⁸ Comprehensive treatment of the thermal vs. electrical rooftop space capacity problem is likely to present significant analytical challenges, particularly considering the range over which energy demand varies, and the time-dependent carbon intensity of electricity from the grid.

Progressive de-carbonization of the residential housing sector is a process fraught with difficulty: an ongoing, path-dependent set of optimization problems over which no one decision-maker exercises complete control. Frequently, different classes of decision-makers (for example, property owners and urban planners) disagree over the definition of optimality (i.e., should aesthetic appeal be a consideration in siting renewable energy capacity?). However, at its core, progressive de-carbonization involves realizing the set opportunities for substitution toward the available energy flows with the lowest embodied and emitted carbon, given resource constraints. ***The current push for proliferation of PV ready buildings and PV capacity may***

¹⁹⁴ California Energy Commission. (9 May 2018). *Energy Commission Adopts Standards Requiring Solar Systems for New Homes, First in Nation* [Press Release]. Retrieved from: https://www.energy.ca.gov/releases/2018_releases/2018-05-09_building_standards_adopted_nr.html?platform=hootsuite

¹⁹⁵ Arnette, A. N. (2013). Integrating rooftop solar into a multi-source energy planning optimization model. *Applied energy*, 111, 456-467.

¹⁹⁶ Awad, H., & Gül, M. (2018). Optimisation of community shared solar application in energy efficient communities. *Sustainable cities and society*, 43, 221-237.

¹⁹⁷ Assouline, D., Mohajeri, N., & Scartezzini, J. L. (2018). Estimation of Large-Scale Solar Rooftop PV Potential for Smart Grid Integration: A Methodological Review. In *Sustainable Interdependent Networks* (pp. 173-219). Springer, Cham.

¹⁹⁸ Herrando, M., Ramos, A., Freeman, J., Zabalza, I., & Markides, C. N. (2018). Technoeconomic modelling and optimisation of solar combined heat and power systems based on flat-box PVT collectors for domestic applications. *Energy Conversion and Management*, 175, 67-85.

yield suboptimal results, in terms of total cost per therm delivered in instances where thermal energy could be generated most efficiently using solar thermal systems. A comparison of solar electric heating technologies with solar thermal technologies for a range of structures is necessary to answer this question.

GLOSSARY

Term	Definition
Active system	A solar thermal system that uses pumps to circulate fluids.
Capital cost	The cost of designing and building an energy system.
Community scale energy system	Energy systems that provide multiple residences or structures with power or heat. Thermal systems that serve more than one residence or structure, but are smaller than district scale systems. Electrical systems that range between 0.5-5MW and are grid connected.
Delivery temperature	The temperature of hot water drawn from a fixture of by an appliance
Heat exchanger	A device for transferring heat from one fluid to another.
Heat load	The amount that must be delivered to an object to maintain a constant temperature.
Heat pump	A mechanical-compression cycle refrigeration system that can be used to heat or cool.
Indirect system	A solar thermal system that collects and transmits thermal energy using separate circuits of pipe.
smart grid	Smart grid is the thoughtful integration of intelligent technologies and innovative services that produce a more efficient, sustainable, economic, and secure electrical supply for California communities.
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APPENDIX A: NREL SAM Output Variables

Variable Name	Units	Description
Energy saved	W	Energy saved by the solar water system.
Hot water draw	kg/hr	The hourly usage of hot water specified in the draw profile on the input page.
Irradiance - Beam	W/m ²	Direct normal irradiance value from the weather file.
Irradiance - Diffuse	W/m ²	Diffuse horizontal irradiance value from the weather file.
Irradiance - Incident	W/m ²	The total hourly incident global irradiance incident on the collector.
Irradiance - Transmitted	W/m ²	The total hourly radiation that makes it into the collector. Depends on the optical properties of the collector.
Operation mode		1 - startup mode, useful energy is collected and tank temperature is somewhat stratified. 2 - mixed mode, useful energy is collected and tank temperature is fairly uniform. 3 - stratified mode, no useful energy is collected and tank temperature is very stratified.
P pump	W	Electric pump power required to drive the collector loop and heat exchanger loop.
Power generated by the system	kW	Equivalent to the energy saved by the system, expressed in kW. When you run the solar water heating model with a financial model, this is the value used by the financial model.
Q auxiliary	W	Electric power required by the auxiliary heater to raise the water temperature from the solar storage tank to the set temperature: $Q_{aux} = \dot{m}_{draw} C_p (T_{set} - T_{deliv})$, where T_{deliv} is the temperature of the water delivered from the solar tank. Because solar heat has been added to the water, $T_{deliv} > T_{mains}$, and less power is needed to bring the water to the desired set temperature than would be required without the solar water heating system.
Q auxiliary only	W	Electric power that would be required without the solar water heating system: $Q_{aux,only} = \dot{m}_{draw} C_p (T_{set} - T_{mains})$.
Q delivered	W	Thermal power delivered by the solar water heating system.
Q loss	W	Envelope loss to room: $Q_{loss} = UA_t (T_{tank} - T_{room})$.
Q saved	W	Electric energy saved by the solar water heating system: $Q_{saved} = Q_{aux,only} - Q_{aux} - P_{pump}$. This value is equivalent to the energy delivered by the solar water heating system.
Q transmitted	W	Solar irradiance transmitted through the collector glass, accounting for collector area: $Q_{transmitted} = I_{transmitted} * A_c$, where $I_{transmitted}$ is the transmitted irradiance and A_c is the total collector area.
Q useful	W	Power delivered by the collector to the solar water storage tank.
Shading losses %		Percent loss of incident beam irradiance due to shading, determined by the shading factors that you specify on the Solar Water Heating page.

T ambient	°C	The mid-hour ambient temperature calculated by averaging the end-of-hour temperature from the previous hour with the end-of-hour temperature from the current hour in the weather file.
T cold	°C	The temperature of the cold portion of the solar storage tank volume in stratified mode. If the tank is not stratified, this value is equal to the previous hour's cold temperature.
T delivered	°C	The temperature of the water delivered from the storage tank.
T hot	°C	The temperature of the hot portion of the solar storage tank volume in stratified mode. If not stratified, this value is equal to the previous hour's hot temperature.
T mains	°C	The temperature of water incoming from the supply source.
T tank	°C	The mean temperature of the solar storage tank.
V cold	m ³	The estimated volume of the cold portion of the solar storage tank, where "cold" is with respect to the hot portion of the tank. SAM models the hot and cold portions as separate nodes. The cold volume increases as users draw water from the tank and mains water replaces it.
V hot	m ³	The estimated volume of the hot portion of the solar storage tank, where "hot" is with respect to the cold portion of the tank. SAM models the hot and cold portions as separate nodes. The hot volume increases from hour to hour as the useful energy from the collector is added until the hot volume is equal to the tank volume (and cold volume is zero).

APPENDIX B: Name of Appendix

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